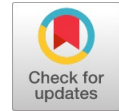


Singularity Analysis of 3 DOF Parallel Manipulators for Angular Drilling in Medical Applications



Arockia Selvakumar A

Abstract: This paper focuses on two 3 – PRS (Prismatic – Revolute – Spherical) parallel manipulators (PMs) carried out by considering three type of singularities. For the study, pin joint forces and torques, linear displacement of nut and mobile platform (MP) tilt of TRIPOD and TRI-GLIDE PMs are taken as important parameters. The singularity positions of the parallel manipulators are simulated in ADAMS environment. The geometrical parameters of the parallel manipulators are considered in logical approach. Based on the results, the concluding remarks are summarized at the end to design the 3 - PRS parallel manipulators with better singular positions for angular drilling in medical applications.

Keywords: ADAMS, Parallel Manipulator, Singularity, TRIPOD, TRI-GLIDE

I. INTRODUCTION

In recent years, the robotic industry needs Parallel Manipulator for machining and manufacturing process due to higher precision, robustness, stiffness and load-carrying capacity [11][12][13][15][16][17]. Most of the PMs kinematics solutions are affected due to their structure or configuration in singular position [1]. PMs precision and control will be lost at singularity condition and PM will gain one or more DOF. Based on the geometrical parameters base, legs and planes, three types of singularity analysis were presented using forward and inverse Jacobian for the non identical 3 DOF PMs and the PMs designs are used in Parallel kinematic machines and Simulators [2]. The PM performance is improved by reshaping the singularities with the help of redundant actuation [5]. In singularity analysis, joints like Translation (T) and Rotational (R) are used to achieve PM motion range by proposing various joint assembly configurations [6]. Similarly, the singular configurations and conditions are found based on the displacements of joints [8]. Clustering algorithm and local routing methods are proposed to achieve PM path planning without singularity [4]. Screw theory is presented with actuation and limb singularities which can be used for the analysis of symmetrical PMs [7]. Grassman-Cayley Algebra

is implemented to analyze the parallel singularities of less than 6 DOF PMs and the singularities are characterized by geometrically [9][10]. Eleven different positions of singularities were shown based on three types of singularities [3]. The position analysis of PMs is carried out by analytical form and the mobile platform motions are found to be zero at direct singularities [11]. Singularity analysis of spherical, revolute PMs is modeled and simulated using a CAD package SMAPS and the results are found to be satisfactory [12].

The singularity analysis and simulation of parallel manipulators have been studied so far in the literature. The papers on the singularity analysis of parallel manipulators accounted for both mobility, work space, and the constraints of the parallel configurations were also considered. The studies of the singularity analysis in the simulation of parallel configurations are very few in the open literature. This work investigates the effect of the mobile platform radius, link length and initial angle between the link and the base platform on the singular positions of some specific parallel manipulator units. By varying one or more of the geometrical parameters of the system, the design of the parallel manipulators can be brought closer to achieve better singular positions. In this paper, the definition of the parallel manipulator and the architectural description of PMs are presented in the following sections. Furthermore, the singularity analyses based on three positions are also explained. This is followed by simulation results of two manipulators are discussed. Finally, the concluding remarks of the comparative study are summarized.

II. ARCHITECTURAL DESCRIPTION OF PARALLEL MANIPULATORS

The 3-DOF Tripod and Tri-glide PMs are shown in Figures 1 and 2. The PMs are typically consisting of a Mobile Platform or Moving platform (MP), Base Platform (BP) and links. The mobile platform is attached to the base platform through joints and links. Revolute joints are used to connect the BP with the links; similarly spherical joints are used to connect the MP with links. The nuts are mounted on the guide ways which consists of two guide rods and a leadscrews. Further the nuts are attached with the revolute joints [12] [13][15][16]. The geometrical parameters of the two PMs are taken by logical approach for the angular drilling in medical applications.

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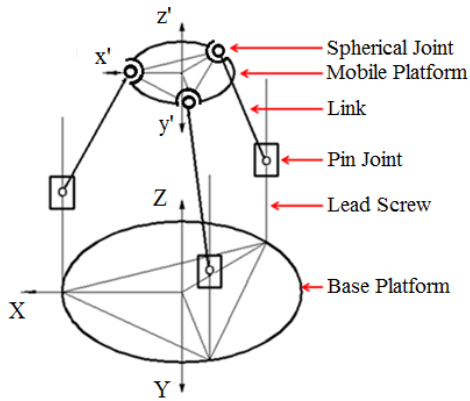


Fig. 1. Tripod PM

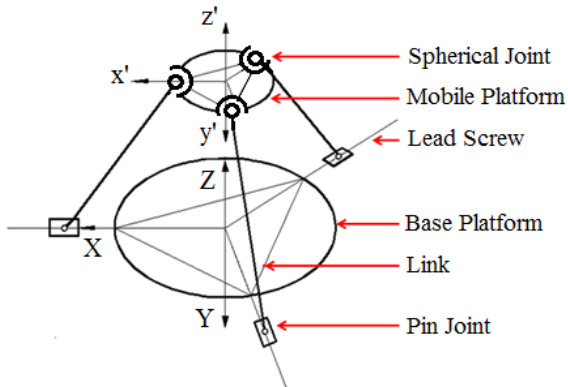


Fig. 2. Tri-Glide PM

III. SINGULARITY ANALYSIS

Singularity is a significant problem in parallel mechanisms, because it leads to loss of controllability and degradation of the stiffness of the system [14][15]. The Figures 3 and 4 shows the schematic diagram of Type I and Type II Singularity positions of PMs [15].

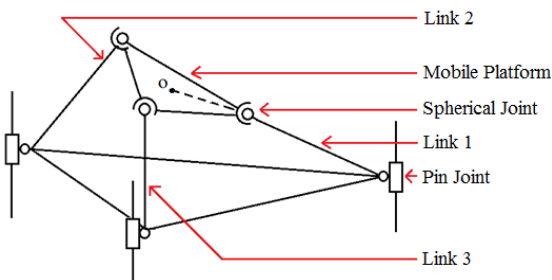


Fig. 3. Singular Poses - Type I Singularity

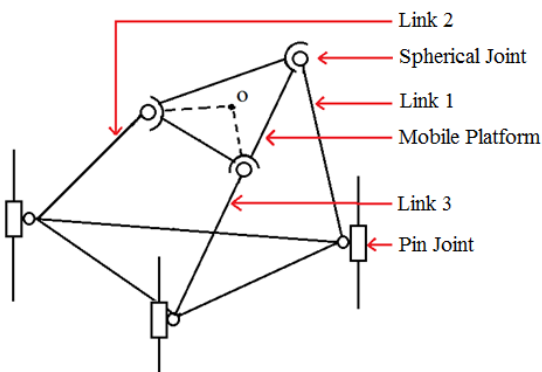


Fig. 4. Singular Poses - Type II Singularity

Type I Singularity position shows the posture of the link 1 and the mobile platform being in the same plane. Similarly, the posture of link 2, link 3 and the mobile platform being in the same plane in the Type II Singularity position [6]. The proposed mechanisms are simulated to find the various singularities, and the positions of the PMs are as shown in Figures 5a to f. Figures 5a and 5d show the first kind (Type I) of singularity of the PRS PMs, when the MP has 180° with any one of the links. Similarly, the MP is in line with the other two links (L2, L3) while link (L1) is kept constant [15]. The second kind (Type II) of singularity of the mechanism is obtained as shown in Figures 5b and 5e. The third kind (Type III) of singularity is obtained when all the links are actuated in different positions to reach the first or second type of singularity position as shown in Figure 5c and 5f. The above mentioned three kinds of singularities are taken in to consideration for the comparative study of the two PMs.

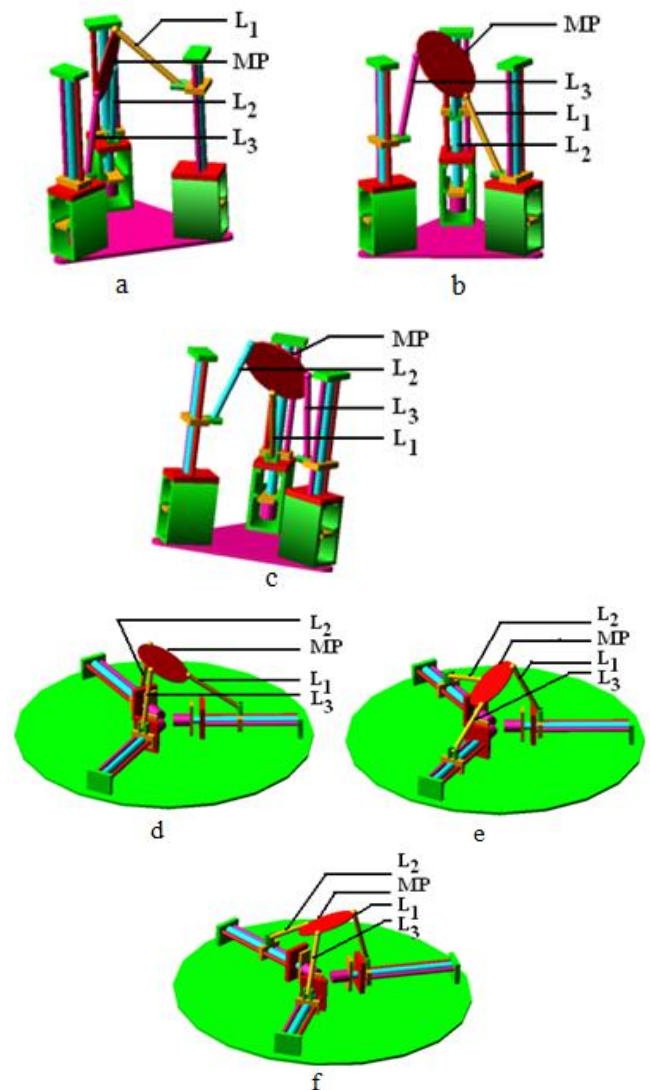


Fig. 5. Three kinds of singularity positions a) Tripod Type I singularity b) Tripod Type II singularity c) Tripod Type III singularity d) Tri-Glide Type I singularity e) Tri-Glide Type II singularity f) Tri-Glide Type III singularity

IV. RESULTS AND DISCUSSION

The Tripod and Tri-Glide PMs are considered for the singularity analysis by considering pin joint forces and torques, linear displacement of nut and Mobile platform (MP) tilt for angular drilling in medical applications. For this simulation study, the geometrical parameters of Tripod and Tri-Glide PMs are considered by logical approach. The geometrical parameters are, MP radius = 90 mm, Link length = 200 mm and the initial angle between the link and the base platform = 77°.

Table 1 shows the simulation results for the two 3-DOF PMs with their MP tilt for the singular positions. From the results, it can be observed that in Type I singularity, the Tripod and the Tri-Glide MP tilts are found to be 78.97° and 34.58° about the X-axis (α). Similarly, in Type II singularity, the Tripod and the Tri-Glide MP tilts are found to be 53.41° and 75.73° about the X-axis. In Type III singularity, the Tripod and the Tri-Glide MP tilts are found to be 8.24° and 10.28° about the X-axis and 59.1° and 30.74° about the Y-axis (β).

Table- I: Results of the MP tilt and nut displacement at singular positions

Parameters	Tripod			Tri-Glide		
	I	II	III	I	II	III
α in °	78.97	53.41	8.24	34.58	75.73	10.28
β in °	0	0	59.1	0	0	30.74
D1 (mm)	200	0	60	94	0	50
D2 (mm)	0	88	120	0	156	100
D3 (mm)	0	88	0	0	156	0

The linear displacement of the nut 1(D1) for the Type I singularity is found to be 200 mm and 94 mm respectively for the Tripod and Tri-Glide PMs. Similarly, the linear displacement of the nuts 2 and 3 for the Type II singularity is found to be 88 mm for the Tripod PM and 156 mm for the Tri-Glide PM. In Type III singularity, the linear displacement of the nuts 1 and 2 is found to be 60 mm and 120 mm for the Tripod PM and 50 mm and 100 mm for the Tri-Glide PM.

Figures 6 and 17 show the result of the pin joints (PJs) force and torque values of the two PMs. From the results, it can be observed that the Tri-Glide PM and the Tripod PM have the joint force of 117 N and 8.84 N for Type I singularity. Similarly, for Type II singularity the Tri-Glide and Tripod PMs have 288.99 N and 24 N. For the Type III singularity Tri-Glide and Tripod PMs have 54.32 N and 35 N.

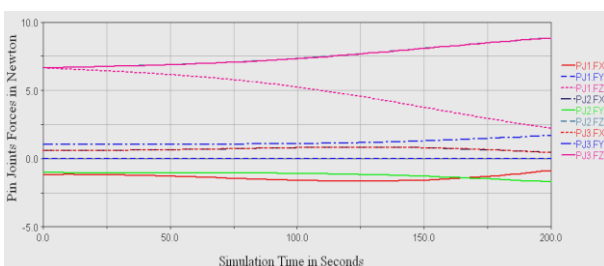


Fig. 6. Type I singularity pin joints force (Tripod)

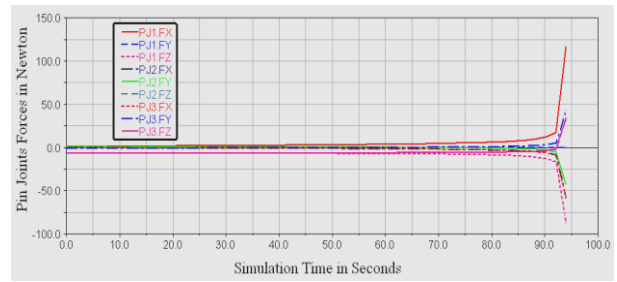


Fig. 7. Type I singularity pin joints force (Tri-Glide)

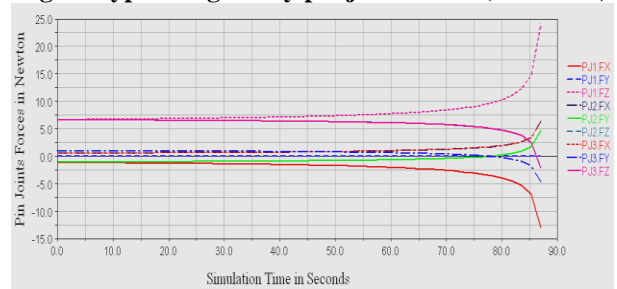


Fig. 8. Type II singularity pin joints force (Tripod)

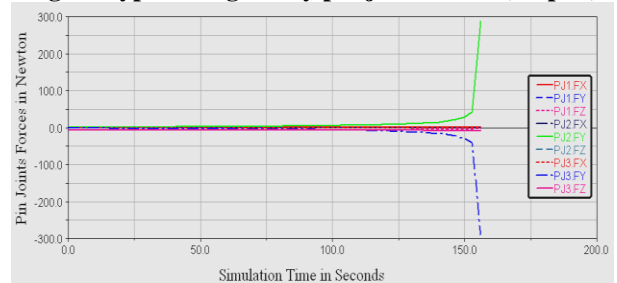


Fig. 9. Type II Singularity pin joints force (Tri-Glide)

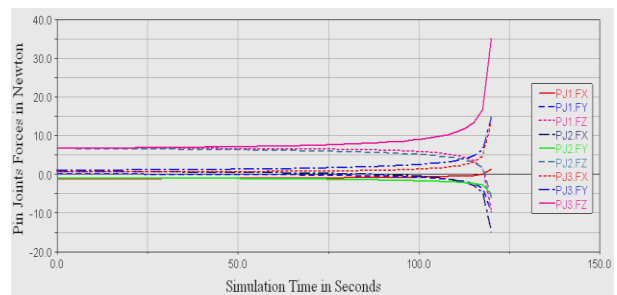


Fig. 10. Type III singularity pin joints force (Tripod)

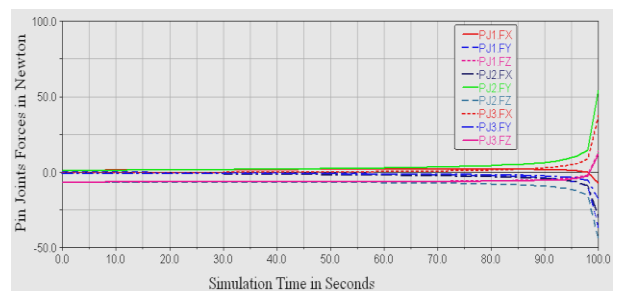


Fig. 11. Type III singularity pin joints force (Tri-Glide)

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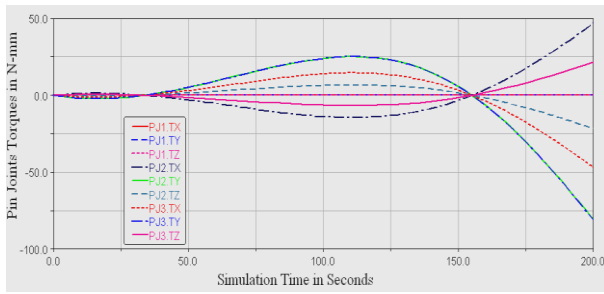


Fig. 12. Type I singularity pin joints Torque (Tripod)

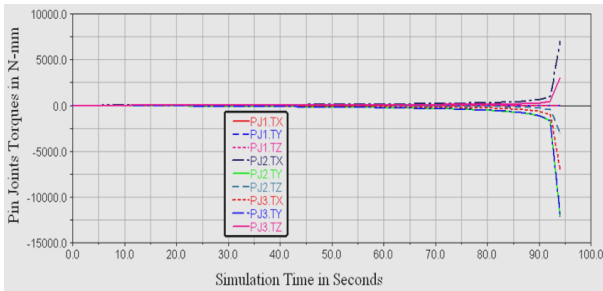


Fig. 13. Type I singularity pin joints torque (Tri-Glide)

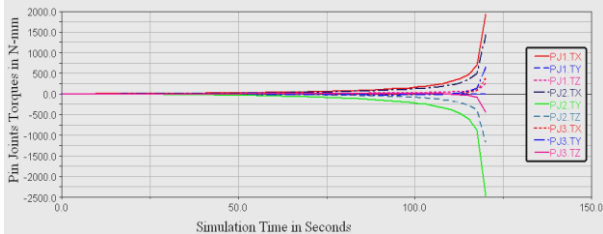


Fig. 14. Type II singularity pin joints torque (Tripod)

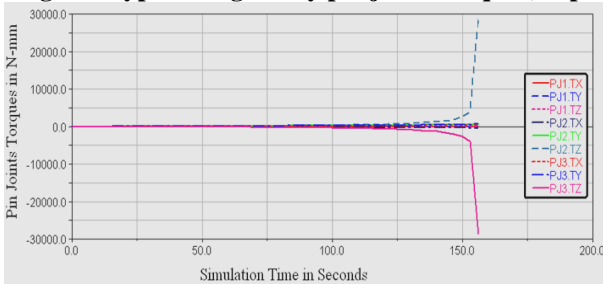


Fig. 15. Type II singularity pin joints torque (Tri-Glide)

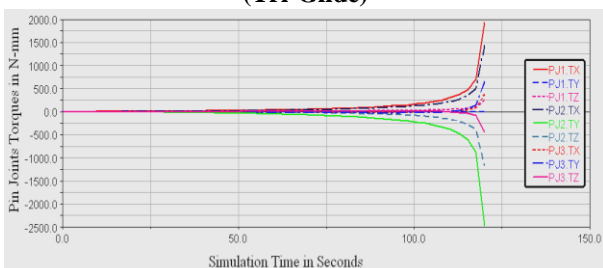


Fig. 16. Type III singularity pin joints torque (Tripod)

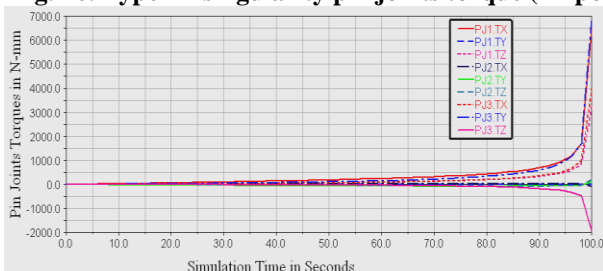


Fig. 17. Type III singularity pin joints torque (Tri-Glide)

Similarly, the pin joints torque values of the Tri-Glide and Tripod PMs are found to be 12056.90 and 80.84 N mm for Type I singularity. For the Type II singularity, the values are found to be 28531.65 and 1336.29 N mm. The pin joints torque values of the Tri-Glide and Tripod PMs, for Type III singularity are found to be 6879.09 and 2459.13 N mm.

V. CONCLUSION

The investigations of this study provided an insight into the singularity analyses of 3-DOF PMs to design a manipulator with better singularity positions. The conclusions of the study based on the three types of singularity positions of TRIPOD and TRI-Glide PMs for angular drilling in medical applications are summarized below.

- From the singularity study, it is observed that the Tri-Glide PM has 53 % lesser linear displacement of the nut than the Tripod PM for the Type I singularity with a single link movement. Similarly, the Tripod PM has 43.5 % lesser linear displacement of the nut than the Tri-Glide PM for the Type II singularity with two links (simultaneous) movement.
- The Tripod PM MP tilt is found to be 56.27 % greater than that of the Tri-Glide PM with single link movement. Similarly, the Tripod PM has 29.47 % lesser MP tilt than the Tri-Glide PM for the Type II singularity with two links (simultaneous) movement.
- In Type III singularity, the MP tilt about the x axis of the Tripod PM is 19.84% greater than that of the Tri-Glide PM. Similarly, the MP tilt about y axis of the Tripod PM is also 48.17% greater than that of the Tri-Glide PM.
- The pin joint torques and forces were simulated for the two Tripod and Tri-Glide PMs. From the results it is observed that, the Tripod PM has 92.44 % lesser pin joint force for Type I singularity, 91.69% Type II singularity and 35.56 % Type III singularity than the Tri-Glide PM.
- The Tri-Glide pin joint forces and torque values are found to be higher than those of the Tripod at the singular positions. This may be due to the larger displacement of nut in the singularity II and III. In Type I singularity, the singular position is obtained earlier than the Tripod structure, but the resisting force due to the non actuated links of the Tri-Glide PM is found to be higher.
- Based on the above concluding remarks, the designer can design the PMs based on his/her requirements.
- Further, the dynamic study of the discussed PMs will be carried out for various types of angular bone drilling in medical applications.

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