Unaccounted Heat Distribution in a Variable Compression Ratio Internal Combustion Engine

Vinay Kumar Yadav, Rajiv Ratan Lal, Dinesh Kumar Soni



Abstract: The compression ratio on heat distribution in an exceedingly variable compression ratio engine. The compression ratio powerfully affects the operating method and provides an exceptional degree of management over engine performance. Variable Compression quantitative relation (V.C.R) engine check rig is employed to see the result of Compression ratio (C.R) on the performance and emissions of the engine and also the distribution of warmth during a variable compression ratio engine. The performance frequency parameters like efficiencies, power adopted, and specific fuel consumption square measure determined. Further, combustion development is additionally discovered through this work, we will notice the optimum compression ratio that the simplest performance is feasible. So as to search out optimum compression ratio, experiments were dispensed on one cylinder four stroke variable compression ratio diesel motor. Tests were dispensed at compression ratios of fifteen, 16, 17.5, 19 and 21 at totally different masses the performance characteristics of engine like Brake power (BP), Brake Thermal potency (BTE), Brake Specific Fuel Consumption (BSFC). Results show a major improved performance at a compression ratio twenty one. The compression ratios lesser than 21 showed an increase in brake thermal potency, come by fuel consumption. The warmth is that the governing issue that operates whole engine and turn out power. Compression ratio between 19 to 21 provides optimum results in distribution of unaccounted heat also improves thermal performance of engine, Each fuel within the world is employed to supply certain quantity of warmth by either mechanical or chemical action. The heat is created by fuel is employed to reciprocate piston within combustion chamber and this reciprocatory motion is regenerate to movement power to regulator by exploitation crank and rod mechanism.

Keywords : Diesel engine, variable compression ratio, performance, Fluid flow, Air-fuel mixture, Intake-valve efficiency, emission, working process..

I. INTRODUCTION

The quantity of cars primarily within the quality of vehicles and business will increase the assembly. The researchers are sorting out on substitute approaches for you to form certain a

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cleaner combustion as results of performance of quality systemshas been taken awareness unremarkably until currently. Withal, confined thermal systems of spark ignition engines (SI) on account that of restricted compression magnitude relation attributable to knock and drawback to diminish material (PM) and oxide (NOx) emissions of compression ignition engines (CI) at the same time place into effect the researches to form replacement choices to broaden engine powerfulness and reduce exhaust emissions. Temperature combustion modes kind of like uniform value compression ignition (HCCI), partly premixed compression ignition [6, 7], reactivity controlled combustion ignition (RCCI) promising combustion modes providing higher thermal powerfulness and at the same time scale down PM and Nox emissions. Variable compression magnitude relation (VCR) could be a any promising technological power to run the engine at the most applicable purpose in phrases of power and emission [1]. Many of the previous stories regarding the consequences of the Cr on HCCI engine are constant quantity researches work the have an impact on of cr on ignition delay, SOC, IMEP then on. Yet operation reasonably the HCCI engine could be an any valuable side that's limiting the utilization of the engine. Brake sure fuel consumption and operation maps also are vital to manage the engine whereas switch between HCCI modes to ancient SI or DI mode [1]. Compression ignition engines supply superior fuel financial system. yet, in diesel engines utilizing mixing-managed combustion strategies, reaching discounts in exhaust emissions stays a priority, since a turbulent diffusion flame surrounds the gas spray, manufacturing nitrogen oxides (NOx) at constant time as soot forms within the rich crucial response space of the gas spray, with soot concentrations increasing on condition that the spray is transported downstream . there is not a flame sector among the tip of the gas contraption and therefore the topmost circulation of the spray combustion during a turbulent diffusion flame, and therefore the amount of the neighborhood (from the contraption to the flame, the other place termed lift-off length or here set-off length) performs a full-measurement operate within the combustion and emission procedures as heaps air is entrained and combined with the gas upstream of the set-off interval [3]. Dominant the set-off amount in conserving with engine operating circumstances is principal to optimize the air-entrainment into the fuel spray.

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2149

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Factors moving the set-off amount [2] additionally because the information of the flame set-off had been staggeringly studied. it's emerge as originated that reducing close density with low boosting and what is more the element awareness with higher exhaust gas recirculation (EGR) makes it potential to increase the set-off size. However, at excessive load operations, it is a ways needed to expand consumption air with high boosting and fewer EGR that shortens the set-off interval. A viable thanks to manipulate the structure length is changing the gas reactivity, because the set-off size is powerfully related with the ignition shelve. Once you think about that this, the low reactivity of fuel is an appealing feature to broaden the set-off length, and therefore the authors have applied gas to compression ignition engines. This manner of combustion system termed gas compression ignition (GCI) has attracted increasing attention as a chance to diesel engines thanks to the capability of low emissions and high thermal potency [8]. This system is okay to ignition management as a result of the combustion phasing is rigorously coupled to the injection temporal order. yet, partaking in ignition manage over an intensive type of engine plenty and rotation speeds continues to be arduous because the ignition temporal order of the GCI powerfully depends at the gas big variety and therefore the time when of injection, and an additional manner to control the ignition temporal order, that is neutral of the injection temporal order, would be needed. One manner to gather that's to form use of 2 fuels that have precise relativities as applied in reactivity managed compression ignition (RCCI) engines [2], however this methodology needs two fuel tanks that makes it tough to enforce in engine programs used for transportation. Depleting fossil fuel reserves, developing fossil fuel costs, danger to the atmosphere from exhaust emissions and world warming wishes a vast international curiosity in developing substitute on fossil fuel fuels for engines [3]. it's determined that the vegetable oils are promising fuels on condition that their homes square measure appreciate that of diesel and square measure created out of crops with marginal attempt [5]. Vegetable oils are merely on the market in rural regions, are renewable, have a moderately excessive cetane selection will be utilized in diesel engines with convenient changes and should even be with ease mixed with diesel throughout the neat and esterified (Biodiesel) forms. Jatropha oil, Karanji oil, vegetable oil, vegetable oil, oil and neem tree oil are a number of the vegetable oils which could be used as fuels in burning engines [4]. The biodiesel from the higher than mentioned vegetation, behave during a totally different methodology in diesel engines in phrases of overall performance, emission and combustion. As on date, a number of experiences works had been administered on biodiesel combustion, total potency and emissions [5 - 9]. Many oil esters observed as biodiesel is tried as replacement to diesel gas [10 - 16]. The engines witnessed larger performance with reduction in smoke, organic compound and CO (carbon monoxide) emissions and expand in Roman deity (nitrogen oxides) emission for the complete higher than recounted situations. [7].

I. MATERIALS AND METHODS

In this study the variable compression engine was run with diesel at completely different compression masses to gauge the performance with unaccounted heat at exhaust. The results were compared between the unaccounted heats, compression ratio, heat loss to engine cooling water, heat unaccounted, yet as for various compression ratios and masses.

II. EXPERIMENTAL SETUP

Commercial diesel fuel utilized in India has been taken for bottom line reading for this study. The take a glance at engine used is variable compression relation multi fuel engine and eddy current measuring instrument. The exhaust gases like HC, CO, greenhouse gas unit measured by the infrared mensuration and various constituent Nox unit measured by Electro chemical detector. This study was administered to research the unaccounted heat throughout exhaust and engine cooling. Below shown table shows the specification of the experimental engine setup. Associate electrical measuring instrument was accustomed apply load on the engine. Tests were administered for a load of 25 N-m, starting from no load to full load condition. At a load of twenty 5 N-m for various compression relation the fuel rate and so the assorted effects of unaccounted heat were analyzed. Processed information acquisition system is employed to gather, store and analyze the info throughout the experiment by mistreatment varied sensors.

| Tested engine specifications. | | | | | |
|-------------------------------|-----------------------|--|--|--|--|
| Item | Value | | | | |
| No. of cylinders | 1 | | | | |
| Bore, mm | 95 | | | | |
| Stroke, mm | 85 | | | | |
| Connecting rod length, mm | 156 | | | | |
| Capacity, cc | 582 | | | | |
| Maximum speed, RPM | 3000 | | | | |
| Engine type | Four Stroke (Variable | | | | |
| | Compression Ratio) | | | | |
| Compression ratio | From 12:1 to 22:1 | | | | |
| Injection timing, deg. BTDC | 20 | | | | |
| Maximum power, KW | 9.5 | | | | |
| Maximum torque, N.m | 45 | | | | |

III. TEST PROCEDURE

The variable compression ratio engine out there within the laboratory is initiated by mistreatment automatic electric motor crank start. Once the engine reaches the operational condition load is applied. The check is conducted at variable speed. Experiment was administered on a check engine running on diesel, with compression ratio of 15, 16, 17.5, nineteen and 21 in order to research the result of unaccounted heat. All the experiments were meted out at constant injection pressure of 200 bar by variable the load from zero to 16.5 kg. Once completion of each experiment the engine was run on diesel thus on flush out fuel in pipe. Exhausts unaccounted heat were measured with measuring instrument a 5 gas MRU delta exhaust gas instrument were accustomed predict impact of emissions.

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IV. ERROR ANALYSIS

Errors and uncertainties at intervals the experiments can arise from instrument alternative, condition, standardization, setting, observation reading and take a glance at developing with. Errors will creep into all experiments despite the care that's exerted. Uncertainty analysis is needed to prove the accuracy of the experiments. In any experiment, the final word results calculated from the primary measurements. The error at intervals the effect is equal to the utmost error in any parameter accustomed calculate the result (Holman) share uncertainties of various parameters like total fuel consumption, brake power, brake specific fuel consumption and brake thermal efficiency was calculated practice the proportion uncertainties of various instruments utilized within the experiment. For the quality values of errors of various parameters given in below shown Table, practice the principle of propagation of errors, the complete share uncertainty of an experimental trial area unit usually computed.

| Uncertainty in measurements and calculated results | | | | | |
|---|-----|----|--|--|--|
| Item Uncertainty Uncertainty Maximum Maximum uncertainty [%] | | | | | |
| Speedrpm | ±10 | ±1 | | | |

| Torque | ±0.2 s | ±1.4 |
|--------|--------|------|
| Time | ±1 | ±1.8 |
| BSFC | - | ±2 |
| BTE | - | ±2 |

V. RESULT AND DISCUSSION

A. Engine Torque

The torque values of various compression magnitude relations are foretold. It's determined that the torque of the warmth minimized because the compression magnitude relation will increase. The explanations behind that are because of the augmented effective and correct combustion. Compared to the opposite compression ratios. The torque values for compression ratios sixteen, 17.5, 19, 21 were in vary of 16.2-20.2, 16-20 and 15.3-18.7 Nm. Thus, increasing the compression quantitative relation had additional edges with unaccounted heat, because of their effectiveness of low volatility and better viciousness in fuel throughout compression.

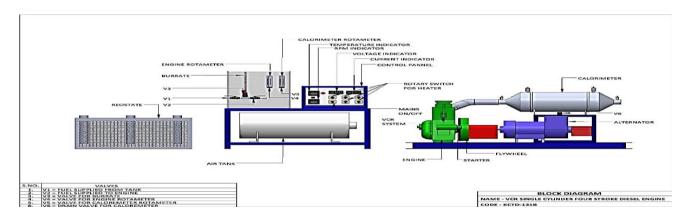


Figure 1.1 – Block diagram of Variable Compression Engine



Figure 1.2 – Experimental setup and test rig of Variable Compression Engine



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B. Brake Thermal Efficiency

The brake thermal efficiency (BTE) performance of compression magnitude relation and completely different compression ratios are shown in Table. BTE of the compression magnitude relation 21 decrease unaccounted heat by 18.6% as compression magnitude relation exaggerated from 14 to 21. Compression magnitude

relation of 21 performance improvement at unaccounted heat and improves brake thermal potency higher compression magnitude relation is because of the entire combustion attributable to effective combustion. The compression magnitude relation of twenty one was found to be the simplest for all cases of unaccounted heat and combustion. Increasing the compression from 15 to 21, will increase the BTE.

| Distribution of Heat at 25 N-m load with variable Compression Ratio | | | | | | | | |
|---|-----------------------------------|-------|-------|-------|-------|-------|--|--|
| | Compression Ratio | 17.5 | 16 | 15 | 19 | 21 | | |
| Н | Heat Supplied By Fuel | 100 | 100 | 100 | 100 | 100 | | |
| Heat Ba | Heat Equivalent to Brake Power | 26.73 | 26.51 | 28.73 | 28.85 | 29.99 | | |
| alance | Heat loss to Exhuast Gases | 24.05 | 35.22 | 43.25 | 41.76 | 41.04 | | |
| e Sheet | Heat Loss to Engine cooling water | 13.47 | 16.71 | 19.33 | 19.26 | 20.34 | | |
| et | Heat Unacconted | 35.75 | 21.57 | 8.69 | 10.13 | 8.63 | | |

| Specific fuel consumption and efficiency at 25 N-m load with Variable compression ratio | | | | | | | | | |
|---|---------------------------------|--------------|----------|--------|--------|--------|--------|--------|--|
| CR | Compression Ratio | Abbreviation | Unit | 15 | 16 | 17.5 | 19 | 21 | |
| Dynamometer | Torque | Т | N-m | 25.00 | 25.20 | 25.60 | 25.30 | 25.50 | |
| | Brake Terminal Efficiency | ŋb | % | 28.73 | 26.51 | 26.73 | 28.85 | 29.99 | |
| Performance parameters | Indicated Terminal Efficiency | ŋi | % | 29.00 | 28.27 | 28.44 | 29.52 | 29.53 | |
| | Brake Specific Fuel Consumption | | gm/Kw-hr | 311.75 | 303.15 | 300.67 | 278.56 | 267.90 | |

| CR | Compression Ratio | Abbreviation s | Unit | 15 | 16 | 17.5 | 19 | 21 |
|-------------------------|---|-----------------------------|----------------|------------|------------|------------|------------|----------|
| | Water Inlet Temp. to Calorimeter | $\mathrm{T}_{\mathrm{wic}}$ | Degree Celsius | 24.10 | 23.50 | 23.30 | 24.50 | 24.4 |
| | Water Outer Temp. from Calorimeter | T_{woc} | Degree Celsius | 40.80 | 38.20 | 33.00 | 39.90 | 40.0 |
| Temperature points E | Exhaust Gas Outer Temp. from Engine | T _{goe} | Degree Celsius | 516.1 0 | 495.0 0 | 414.8 0 | 492.6 0 | 473 0 |
| | Exhaust Gas Inlet Temp. to Calorimeter | T_{gic} | Degree Celsius | 334.1 0 | 302.0 0 | 238.9 0 | 323.7 0 | 319 0 |
| | Exhaust Gas Outlet Temp. from Calorimeter | T_{goc} | Degree Celsius | 134.3 0 | 110.3 0 | 85.90 | 142.2 0 | 135 0 |
| | Water Inlet Temp. to Engine | $\mathrm{T}_{\mathrm{wie}}$ | Degree Celsius | 24.10 | 23.50 | 23.30 | 24.50 | 24.4 |
| | Water Outer Temp. from Engine | T _{woe} | Degree Celsius | 42.40 | 39.80 | 36.60 | 43.10 | 45.0 |
| | Water Flow Rate - Engine | Mw | LPH | 125.3 0 | 131.1 0 | 130.1 0 | 123.0 0 | 114 0 |

2152



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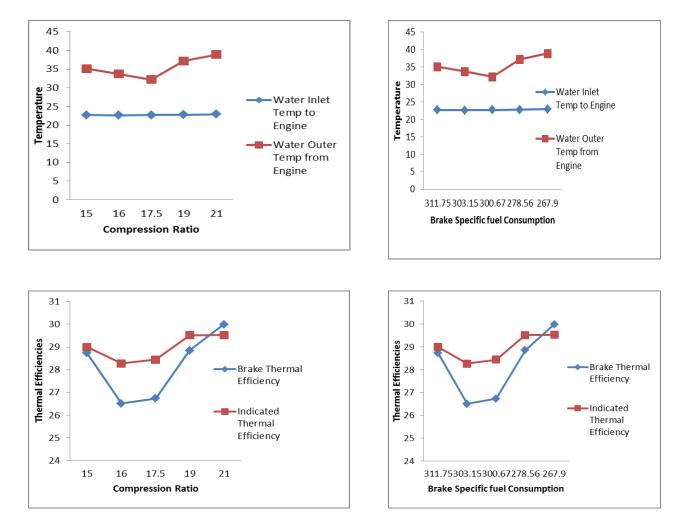


Figure 1.3 – Representation of unaccounted heat observed during testing

VI. BRAKE SPECIFIC FUEL CONSUMPTION

The Brake specific fuel consumption for compression relation of 21 at load of 25 masses for varied unaccounted heat areas. It's obvious from the figure that BSFC of the engine step by step decreases with the increase in load. BSFC for compression relation 21:1 is comparatively below different compression ratios of 15:1, 16:1, 17.5:1. At higher compression relation and higher load the energy required per increase in load. By increasing the compression relation of the engine, the brake thermal efficiency put together gets raised.

| Compression Ratio | 17.5 | 16 | 15 | 19 | 21 |
|---------------------------------|--------|--------|--------|--------|-------|
| Torque | 25.6 | 25.2 | 25 | 25.3 | 25.5 |
| Brake Thermal Efficiency | 26.73 | 26.51 | 28.73 | 28.85 | 29.99 |
| Indicated Thermal Efficiency | 28.44 | 28.27 | 29 | 29.52 | 29.53 |
| Brake Specific fuel Consumption | 300.67 | 303.15 | 311.75 | 278.56 | 267.9 |
| Water flow rate-Calorimeter | 125 | 125 | 125 | 125 | 125 |
| Water Inlet Temp to Engine | 22.7 | 22.6 | 22.7 | 22.8 | 22.9 |
| Water Outer Temp from Engine | 32.2 | 33.7 | 35.1 | 37.2 | 38.9 |



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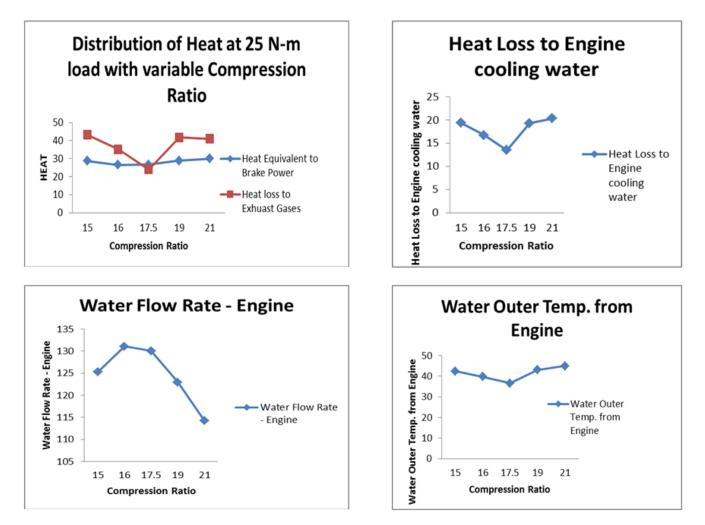


Figure 1.3 – Representation Of Temperature Distribution Observed During Testing

VII. CONCLUSIONS

Performance Analysis of variable compression ratio 15, 16, 17.5, 19 and 21 the following conclusions are withdrawn:

1) Brake Thermal potency (BTE): Result table shows that the most brake thermal potency is obtained at a compression magnitude relation of 21; the smallest amount brake thermal potency is obtained at a compression magnitude relation sixteen. Hence, with reference to brake thermal potency, twenty one will be treated as optimum power output. This will be attributed to higher combustion and better intermixing of the fuel and air at this compression magnitude relation.

2) *Fuel Consumption:* the higher fuel consumption was obtained at a compression magnitude relation of fifteen (Result Table). The upper and lower compression ratios than 15 resulted in high fuel consumption. The fuel consumption at a compression magnitude relation of sixteen and 17.5 was virtually the minimum distinction fuel consumption. The high fuel consumption at higher compression ratios will be attributed to the result of charge dilution. At the lower sides of the compression ratios, the fuel consumption is high because of incomplete combustion of the fuel.

3) Specific Fuel Consumption: the higher specific fuel consumption was obtained at a compression magnitude relation of 15 and lower compression ratios than 15 resulted in high specific fuel consumptions. The precise fuel

consumption at a compression magnitude relation of 16 and 17.5 was virtually the minimum distinction fuel consumption. At the lower sides of the compression ratios, the precise fuel consumption is high because of incomplete combustion of the fuel. the higher specific fuel consumption was obtained at a compression magnitude relation of 15 and lower compression ratios than 15 resulted in high specific fuel consumptions. The precise fuel consumption at a compression magnitude relation of 16 and 17.5 was virtually the minimum distinction fuel consumption. At the lower sides of the compression ratios, the precise fuel consumption is high because of incomplete combustion of the fuel.

4) Mechanical Efficiency: The variation in mechanical potency at totally different hundreds for various compression ratios is shown in it's ascertained that mechanical potency will increase with the rise within the load because of increase within the BP and scientific discipline. With the rise in compression magnitude relation the mechanical potency additionally will increase and also the mechanical potency at compression magnitude relation of 15, 16, 17.5,19 and 21 wasn't identical however minimum distinction mechanical potency.

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5) Indicative Mean Effective Pressures: Indicative Mean Effective Pressures were found to be increasing with the rise in load and also the compression magnitude relation. The best Indicative Mean Effective Pressures was recorded for the compression magnitude relation 16 whereas the smallest amount was for 19.

6) Exhaust gas temperatures were found to be increasing with the rise in load and also the compression magnitude relation. The highest exhaust gas temperature was recorded for the compression magnitude relation 15 whereas the smallest amount was for 17.5.

7) The optimum compression ratio for unaccounted heat distribution is found between 19 to 21.

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2155