

A Renewable Energy Fed Non-Isolated Inverse Output Voltage DC-DC Converter with Broad Range of Conversion

M. Praveen Kumar, P. Maheeth, M. Sai Krishna Reddy, S. Ravi Teja

Abstract: Renewable Energy fed non-isolated negative output Converter with dc-dc conversion is proposed which employed for various applications. In industrial purposes only few converters are available for wide conversion ratio, the proposed design has come up with wide range negative voltage load applications. The proposed converter is analyzed and design for continuous condition mode. For verification of theoretical analysis, the proposed converter is simulated using PSIM 9.0.

Index Terms: Negative output, Wide Gain, Buck-Boost, Non-isolated.

I. INTRODUCTION

DC-DC converters plays significant role in manufacturing requirements since their usage is inevitable. Applications mainly like inverting charge pump, audio amplifiers, digital camera, in hybrid electric vehicles for regeneration purpose of dc motors (RBS), buck-boost voltage inverter, for generation of wind power and power generation from photo voltaic. [1]-[4], etc.

As familiar as there are two typical traditional converters, they are traditional buck-boost converter and CUK converter gives a reverse output. Where D is the duty cycle and their conversion ratio of voltage is $(-D/(1-D))$ is same. They can produce the output voltage has higher or lower compared to the input voltage. Hypothetically, these converters will produce the output voltage as weather high step-up or step-down. Duty cycle is approximately equal to 0 or 1, still real-world operation. This condition will not be met for the diodes and the power switches [5]-[6]. A transformer will be used for fly-back converter to get wide conversion ratio of an output voltage. The switch voltage of the transformer will be exceeding, and EMI difficulties occurs, and which causes for low efficiency and vast volume [7]. Vast number of Inverse output converters have been suggested in this past decade, suppose, the voltage conversion ratio $M(d) = -D$ for the topology of the inverse output KY buck-boost converter who had the fast load transient response was suggested in [8]. $M(d) = -2D$ is the voltage conversion ratio for the N/O

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M.Praveen kumar, B.Tech, Dept. of Electrical and Electronic Engineering, KLEF, Vaddeswaram, Guntur,INDIA

Pochanapreddi Maheeth, B.Tech, Dept. of Electrical and Electronic Engineering, KLEF, Vaddeswaram, Guntur,INDIA

M.Sai Krishna Reddy, Asst.Professor,Dept. of Electrical and Electronic Engineering, KLEF, Vaddeswaram, Guntur,INDIA

S.Ravi Teja, Asst. Professor,Dept. of Electrical and Electronic Engineering, KLEF, Vaddeswaram, Guntur,INDIA

KY-Buck-Boost converter who possessed no additive characteristics was suggested in [9].

The topology of the inverse output KY-buck-boost has been built the path for the Boost converter is integrated as positive to inverse with voltage conversion ratio as $-1/(1-D)$ was suggested in [10].

In this paper is planned as following manner. The regulation and stable state analysis of the prompt device area unit outlined in section II. PSIM simulations to verify theoretical analysis are presented in section III. Conclusions are made available at the end of the paper.

II. STEADY STATE ANALYSIS

We can see from Figure 1.1, the suggested converter forms of input voltage v_{in} , from PV panel and two active devices and two passive devices D_1 and D_2 , it consists of two inductors L_1 and L_2 , two capacitors C and C_0 and only single load resistance R. For steady state operation details and analysis of the converter it is assumed to that all the components are ideal, also the inductors and capacitors are large enough to maintain ripple almost negligible and to operate converter in

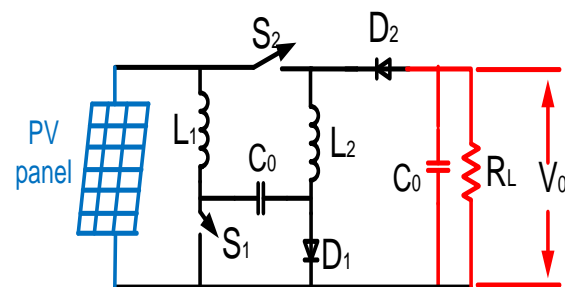


Figure-1.1 Proposed converter circuit diagram

Interval-1 (T_{on} - condition)

During this interval active switches are on and passive devices are in OFF condition. This case equivalent circuit is shown in figure 2. we have derived the voltage across the inductors and current through the capacitors as follows.

$$L_1 \frac{di_{L1}}{dt} = v_{in}$$

$$L_2 \frac{di_{L2}}{dt} = v_{in} + v_c$$

$$C \frac{dv_c}{dt} = -i_{L2}$$

$$C_0 \frac{dv_o}{dt} = -\frac{v_o}{R}$$

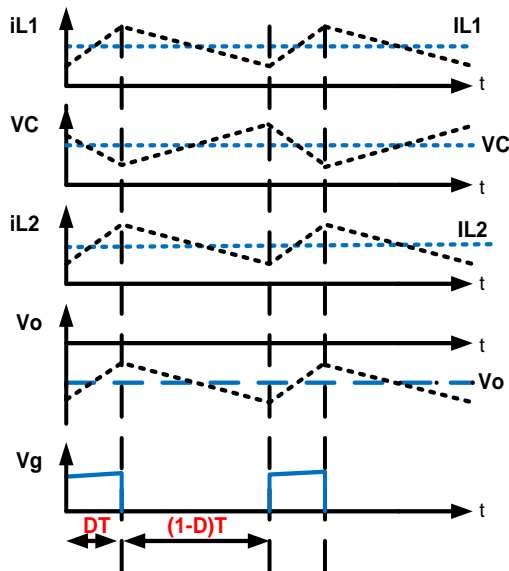


Figure 1.2 shows steady state waveforms of the proposed converter

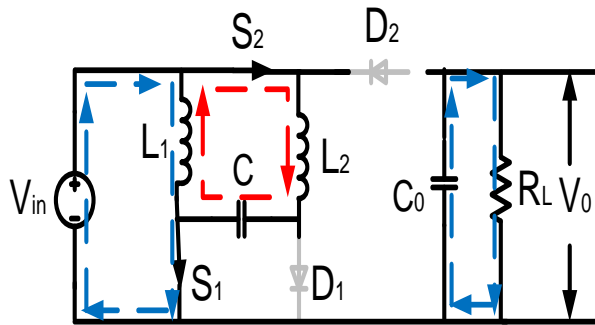


Figure-2 ON state equivalent circuit

Interval-II (T_{off} condition)

During this interval active devices are in off condition and passive devices are forward biased. This case equivalent circuit is shown in figure-3. The voltage across inductors and current through capacitors are derived as follows.

$$L_1 \frac{di_{L1}}{dt} = v_{in} - v_c$$

$$L_2 \frac{di_{L2}}{dt} = v_o$$

$$C \frac{dv_c}{dt} = i_{L1}$$

$$C_o \frac{dv_o}{dt} = -i_{L2} - \frac{v_o}{R}$$

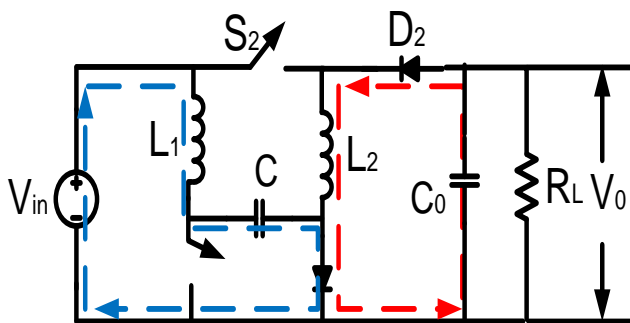


Figure-3 OFF state equivalent circuit

Applying volt-sec balance for both the inductors and solved for relation between input voltage and output voltage as follows.

$$Dv_{in} + ((1 - D)(V_{in} - V_c)) = 0 \quad (1)$$

$$D(v_{in} + v_c) + (1 - D)v_o = 0 \quad (2)$$

Consequently, we have resulting V_c and V_o from (1) and (2)

$$V_c = \frac{1}{(1-D)} V_{in}$$

$$V_o = -\frac{D(2-D)}{(1-D)^2} V_{in}$$

Therefore, we have represented the gain of the suggested converter as

$$M = \frac{v_o}{v_{in}} = -\frac{D(2-D)}{(1-D)^2}$$

Apparently, if the duty cycle D is lesser than 0.29, the voltage gain M is a smaller amount than one, the prompt device works in step down voltage mode in such the simplest way, else it works in boost mode. Whereas the conventional buck-boost converter operates at $D < 0.5$ for buck mode and $D > 0.5$ for boost mode which restricts gain. The below equations represents the blocking voltages of switches and diodes

$$v_{D1} = \frac{v_{in}}{(1-D)}$$

$$v_{D2} = \frac{v_{in}}{(1-D)^2}$$

$$v_{S1} = \frac{v_{in}}{(1-D)}$$

$$v_{S2} = \frac{v_{in}}{(1-D)^2}$$

III. SIMULATED RESULTS

To validate the theoretical analysis and design the proposed converter is simulated in PSIM 9.0.4. The following simulation parameters are taken into consideration which is shown in table-I. The output voltage from PV panel set to 20V and the converter operated in two mode buck mode and boost mode for meeting voltage requirements of signal generator and data transmission applications.

Table-I

Parameters of main circuit

| Specification | Buck Mode | Boost mode |
|--------------------------|-----------|------------|
| PV panel Output voltage | 20 V | 20 V |
| Converter Output voltage | -13.47 V | -105 V |
| Operating frequency | 40 kHz | 40 kHz |
| Load resistor | 10 Ω | 10 Ω |
| Duty ratio | 0.23 | 0.6 |
| Inductor L1 | 0.8mH | 0.8mH |
| Inductor L2 | 1mH | 1mH |
| Capacitor C1 | 10μF | 10μF |
| Capacitor C2 | 44μF | 44μF |

Here the inductor currents in buck mode has shown in Fig-4 and the inductor current ripple during in buck mode is very low. In fig-5 shows the output voltage and intermediate capacitor voltage

during buck mode it can be seen that the voltage ripple of the capacitor is very low. In Fig-6 blocking voltages of the active switches during buck mode which shows low value. In fig-7 inductor currents during boost mode shown having lowest ripple. In fig-8 shows the output voltage and intermediate capacitor voltage during boost mode it can be seen that the voltage ripple of the capacitor is very low. Fig-9 shows blocking voltages of the active switches during boost mode which shows low value.

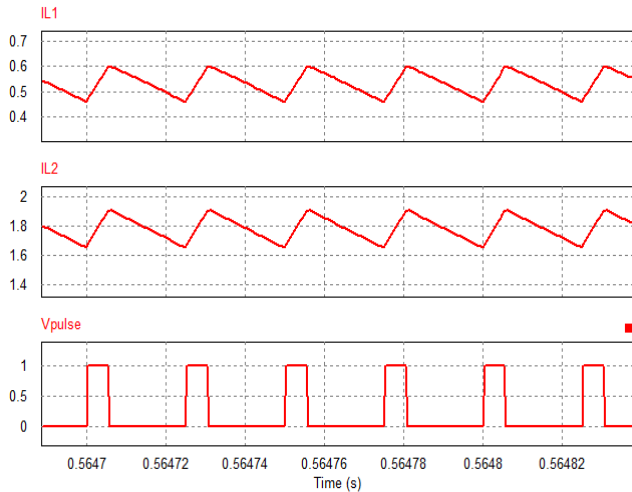


Figure-4 Inductor currents in buck mode

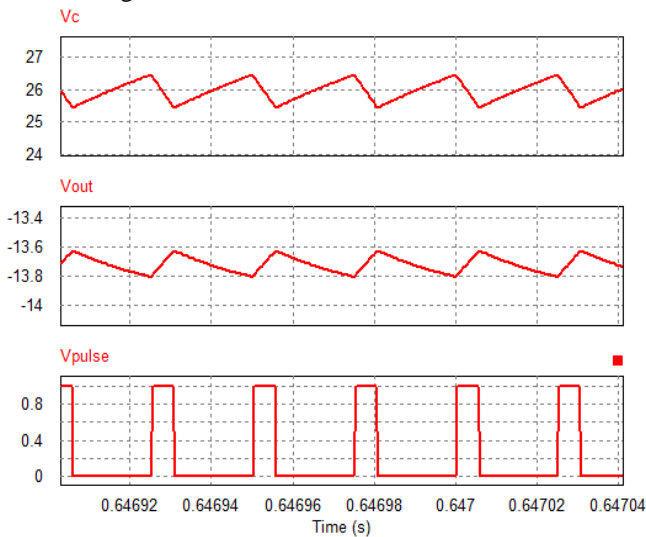


Figure-5 Output voltage and intermediate capacitor voltage during buck mode

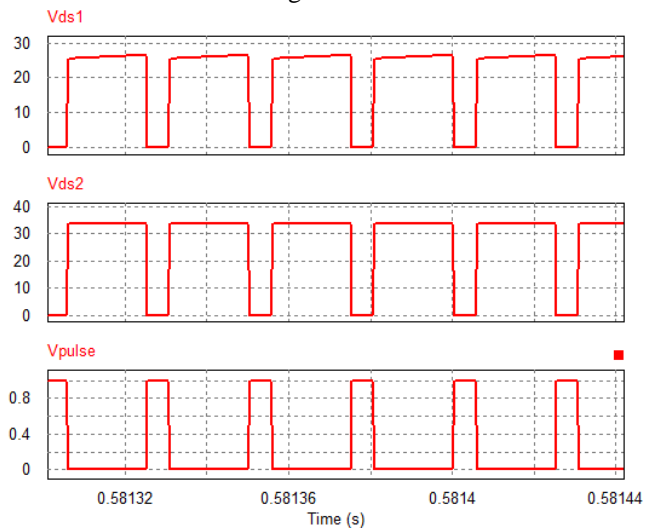


Figure-6: Switch blocking voltage during buck mode

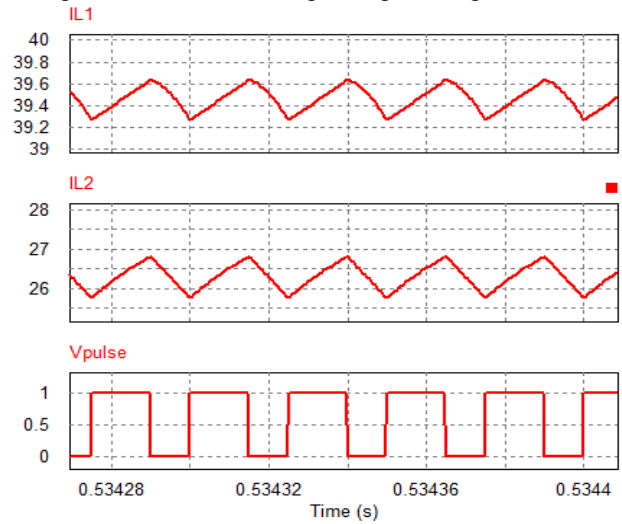


Figure-7 Inductor currents in boost mode

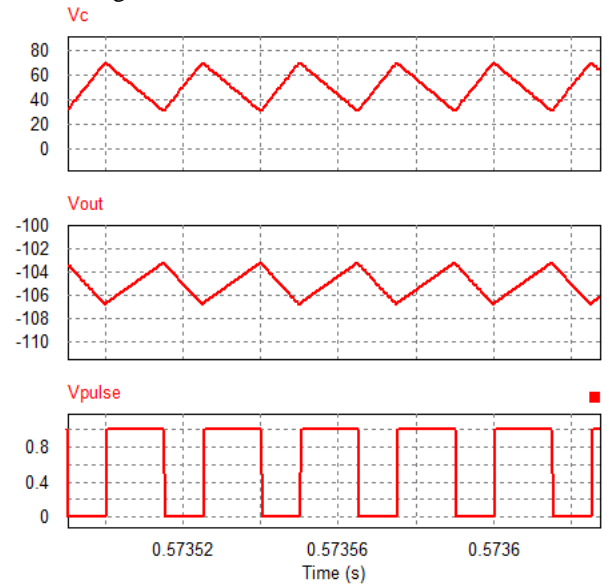


Figure-8 Output voltage and intermediate capacitor voltage during boost mode

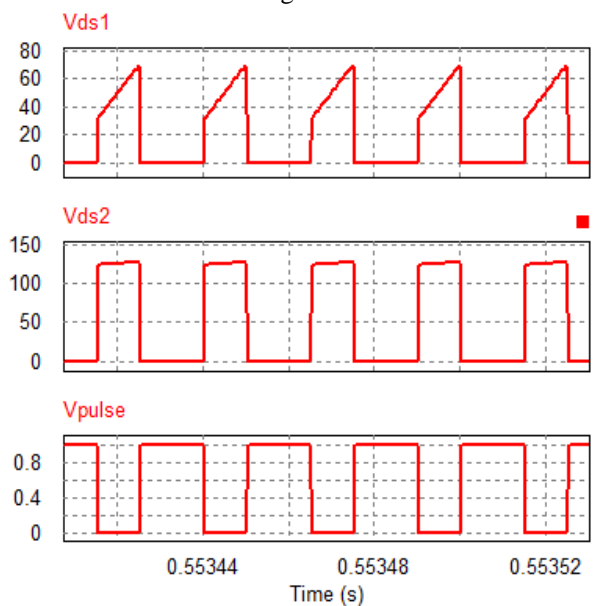


Figure-9: Switch blocking voltage during boost mode

IV. CONCLUSION

A Non-Isolated inverse output for Buck-Boost device is recommended, evaluated and authorized during this project paper. The steady state analysis has been done and the simulations are verified to validate the analysis. It is observed that the proposed converter have highest gain which allows the converter suitable for broad conversion ranges. Also, from results low ripple content can be observed for inductor currents and capacitor voltages which makes component selection easy.

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AUTHORS PROFILE



M.Praveen Kumar was born in Andhra Pradesh, India. He is pursuing his Bachelor's degree in electrical and electronics engineering from KLEF, Vaddeswaram, Guntur. His research interests include electrical drives, power electronics, electric machines, renewable-energy systems, and electrical hybrid vehicles.



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