

Appliance of Soft Switching Scheme over Fuel-Cell based Power Conversion Improvement via Fuzzy Nature

Durgam Kumaraswamy, B.V. Sanker Ram

Abstract: In PV based Solar and Tele-Communication industries power efficient DC-to-DC converters are required to manage the Fuel Cell Systems. These DC-DC converters should be high in power and efficiency as well as it should have low Electro Magnetic Induction [EMI]. The main motto of this systems are to raise the power by using Step-Up Conversion and improving the soft switching ratio. The usage of Coupled inductor and Isolated Transformers are satisfying the needs of higher voltage supply and soft switching scenario. For transforming the electro chemical energy into electrical energy fuel cells are needed, as well as this fuel cells are used to attain high efficiency, lower emitting ratio and speeder operating power while conversion. Several approaches have been already realized to these kind of DC-to-DC power conversion scenarios but failure free scenario of fuel cell systems needs the elimination of bad voltage switchings, requiring higher inputting power as well as large ranging of outputs with higher energy efficiency. For getting out from these faults we need a special Soft Switching nature of MOSFETs and resulting rectifiers. The proposed methodology combines the scenario of Fuzzy logical controllers [FLC] with Soft Switching to attain higher efficiency over fuel cells and its performance improvements over anycase of output strategies. This nature will eliminates the losses os power occurred in switching strategies and reducing the back recovering losses and its nature as well as providing the trustworthy conditions in circuit nature and this kind of design eliminates the large circulations over initial stages. The proposed results will be experimentally proven by using MATLAB SIMULINK and Hardware Circuit Scenarios.

Index Terms: Fuzzy Logic, DC-to-DC, Fuel Cell [FC], Electro Magnetic Induction [EMI], Soft Switching.

I. INTRODUCTION

Fuel Cells are control sources that change over electrochemical vitality into electrical vitality with high effectiveness, low discharges, and calm operation. An essential Proton Exchange Membrane [PEM] single cell course of action is fit for creating an unregulated voltage beneath 1V and comprises of two terminals [Anode and Cathode] connected by electrolyte [1].

The yield current ability of a solitary cell relies on upon the cathode viable territory, and a few single cells are associated in arrangement to shape a Fuel Cell stack. Because of the mechanical difficulties related with stacking a few single cells, Fuel Cell are commonly low-voltage, high current power sources and can constantly run while reactant is sustained into the framework [2].

A few ways to deal with acknowledge DC-DC secluded power change for Fuel Cell control sources have been proposed in view of full extension, push-pull, and current-sustained topologies. A portion of the key commitments in the territory incorporate the investigation laid out in the accompanying. A Fuel Cell control converter in view of a controlled voltage doubler was presented, which utilizes stage move tweak to control the power course through the transformer spillage inductance [3]. This intriguing topology ended up being less effective than other conventional topologies [4], however shows the upside of the low part check. A Fuel Cell inverter in view of a customary push-pull DC-DC converter was exhibited highlighting minimal effort, low part number, and DSP control [5]. In view of the push-pull topology, a particular engineering was displayed to improve adaptability and unwavering quality [6].

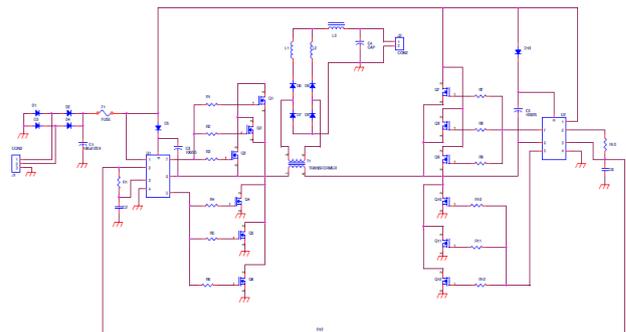


Fig.1. Proposed Circuit Diagram.

An imaginative current-sustained variant of the push-pull topology has been accounted for as a major aspect of a framework associated inverter framework [7]. A comparable current-nourished push-pull topology was utilized in a stage up thunderous converter, showing a high voltage-change proportion [8]. A full-connect forward DC-DC converter with a full-connect rectifier was introduced [9]. This is an exceptionally hearty topology when worked with Zero-Voltage Switching/Exchanging [ZVS] procedure and speaks to an industry standard in numerous applications, for example, telecom control supplies [high input voltage].

Manuscript published on 30 August 2017.

* Correspondence Author (s)

Durgam Kumaraswamy, Research Scholar, Department of Electronics and Electrical Engineering, Jawaharlal Nehru Technological University, Hyderabad (Telangana)-500085, India. E-mail: kumaraswamydurgam77@gmail.com

B.V. Sanker Ram, Professor, Department of Electronics and Electrical Engineering, Jawaharlal Nehru Technological University, Hyderabad (Telangana)-500085, India. E-mail: bvsram342@yahoo.co.in

© The Authors. Published by Blue Eyes Intelligence Engineering and Sciences Publication (BEIESP). This is an open access article under the CC-BY-NC-ND license <http://creativecommons.org/licenses/by-nc-nd/4.0/>

A three-stage adaptation of the full-connect forward converter was as of late proposed [10], in light of Δ -Y transformer association and a cinch circuit to lessen the spillage inductance and circling streams. Another group of stage move ZVS with versatile vitality stockpiling was additionally proposed to increment delicate exchanging working reach utilizing helper circuits [11].

Too, topologies in light of current-nourished full-connect topologies were proposed including low-input swell present and decreased weight on the info side switches [12].

Fruitful power molding for Fuel Cell frameworks requires managing poor voltage control, high information current, and an extensive variety of yield stacking conditions while keeping up high effectiveness and low exchanging anxiety. At the point when presented to these stringent necessities, full-connect ZVS, push-pull, and current bolstered topologies are stood up to with a few specialized difficulties. For instance, keeping up ZVS [Full Bridge] is troublesome because of the poor voltage direction of the Fuel Cell and the extensive variety of stacking conditions, which makes exorbitant conduction misfortunes because of coursing current in the essential.

The push-pull topology decreases transformer use [primary focus tap], bargains polarizing balance as the power rating increments [winding asymmetry and excitation imbalance], and additionally constraining the conceivable outcomes for delicate exchanging operation. Current-bolstered based topologies require massive info inductors [High Current], show motions delivered by the communication between parasite [leakage inductance, intra winding capacitance, and the information inductor], and could exhibit over the top debasing high-recurrence swell current in the yield capacitors because of the nonattendance of channel inductor. While the pattern for high-input-voltage converters [for instance associated with the line] has been to limit exchanging misfortunes and manage generally little line direction, Fuel Cell influence change gives the inverse situation low information voltage, poor control, and high information current. Not at all like applications with high information voltage, accomplishing ZVS with low voltage does not prompt significant productivity increases, given the little vitality put away in the MOSFETs yield capacitance [Coss]. The power scattered in a MOSFET because of the yield capacitance amid turn on is an element of the square of the Fuel Cell voltage $v_{\text{Fuel Cell}}^2$. Since Fuel Cell are low-voltage, high-current power sources, the relative significance of exchanging misfortunes can be exceeded by conduction misfortunes in the MOSFETs that are a component of $i_{\text{Fuel Cell}}^2$.

The fluffy set hypothesis is additionally used to take care of vulnerability issues. The key advantage of fluffy rationale is that its learning portrayal is express, utilizing straightforward "Assuming THEN" relations. All circumstances that are not described by a basic and very much characterized deterministic scientific model, can be all the more effortlessly dealt with as far as the fluffy set hypothesis, in which straightforward principles and various basic participation capacities are utilized to infer the right outcome.

By and large, fluffy sets are effective at different parts of unverifiable information portrayal and are subjective and heuristic, while neural systems are fit for gaining from illustrations, yet have the deficiency of verifiable learning portrayal. The fluffy rationale framework is curved in three

fundamental components: fuzzification, fluffy surmising, and defuzzification. Degrees of enrollment in the fuzzifier layer are computed by IF-THEN guidelines. They construct their choices with respect to contributions to the type of a semantic variable gotten from participation capacities, which are equations used to decide the fluffy set to which an esteem has a place and the level of enrollment in that set. The factors are then coordinated with the particular etymological IF-THEN principles and the reaction of each govern is gotten through fluffy ramifications. To perform compositional lead of induction, the reaction of each manage is weighted by the impedance or level of participation of its data sources and the centroid of the reaction is ascertained to create the suitable yield.

This system delivers the difficulties between [1] and [5] by proposing an arrangement of delicate exchanging systems in a full-connect forward topology. For this reason, a unique balance arrangement is produced to limit conduction misfortunes while keeping up delicate exchanging attributes in the MOSFETs and delicate moves in the yield rectifiers. Helper components in the essential, for example, arrangement inductors and capacitors that are unrealistic to acknowledge due the extraordinary info current are stayed away from by reflecting them to the optional of the circuit to limit circling current and create delicate moves in the switches.

These varieties are reasonably portrayed in Fig. 1 showing three noteworthy alterations suited for Fuel Cell control change. The proposed consolidated strategies can keep up high productivity in the whole working scope of the Fuel Cell [Wide Input Voltage] and under any stacking condition. Itemized examination of the procedures for productivity picks up is exhibited and a stage move ZVS topology is utilized as a source of perspective topology to highlight the systems for execution upgrade and the points of interest in the utilization of the uncommon regulation. Test consequences of a 1-kW control converter are exhibited to approve the proficiency picks up, delineate the advantages of the extraordinary adjustment, and show the delicate exchanging moves.

II. DC-DC VOLTAGE REGULATION OVER FUEL CELL

The low-level unregulated DC voltage given by an energy unit stack is associated with a lift sort DC control converter to venture up the voltage connected to a given load. This yield voltage tends to diminish as more present is requested from the cell. Along these lines, a control plot is required to manage the yield voltage. It is demonstrated that straight, time differing, state input controllers, in light of fundamental inactive yield criticism, following up on correct open circle direction following mistake models of a huge class of energy hardware gadgets, semi-comprehensively balance out the control blunder to zero.

This summary quickly returns to the control normal for a polymer-electrolyte Fuel Cell under various working conditions, giving the premise to fruitful plan of energy molding stages. Both PEMFuel Cell and Direct Methanol Fuel Cell [DMFC] have a place with this classification.

The elements that mostly add to the yield voltage conduct in a DMFuel Cell are fuel [Methanol Focus], fuel stream rate [provided to the anode], air/oxygen stream rate [provided to the cathode], and working temperature [1]. Too, the yield current is a noteworthy element that influences the yield voltage and, thus, its yield control. It is fascinating to take note of how the yield voltage of this DMFuel Cell is significantly influenced by its working temperature and yield current.

[fuel and oxygen stream rates are near ideal for this situation]. This outcomes in a critical change of the accessible yield control, the territory under the polarization bend.

Thusly, with a specific end goal to acquire a coveted yield control, it is first important to adjust the working conditions to build the zone under the polarization bend [for instance, by expanding the working temperature]. It ought to be called attention to that the move from a given polarization bend to another through variety in working conditions is moderate. The primary purposes behind this conduct are the high warmth limit of the cell, and the moderate mass transport forms in the stream fields and cathodes [fuel circulation in the stream channels and terminal gathering] [2], [23]. Be that as it may, a quick unique reaction exists when the yield current changes in settled working condition. Because of this case, the poor voltage control, high present and low-voltage qualities are highlighted. A similar standard takes after for bigger cathode ranges required to create high streams, and various singles cells in arrangement to acclimate a Fuel Cell stack.

III. MODULATION SCHEME OF RIGHT ARRANGED PRIMARY INDUCTION REMOVAL IN FBT

This summary portraits in a successive and calculated way the means taken to satisfy the prerequisites toward expanding the proficiency of the full-connect forward converter in Fuel Cell control transformation. A depiction of the power-misfortune systems in the information arrange is first exhibited, trailed by the examination of the yield rectifier. Each plan objective is tended to by the joined impacts of the proposed delicate exchanging procedures.

A. Input Phase of Full Bridge Topology [FPT]

The conduction misfortunes in the MOSFETs because of coursing current [design objective [a]] and the high-current massive inductor in the essential are wiped out by evacuating the customary Lzvs inductor in the essential and by constraining a privilege adjusted arrangement of heartbeats in the upper switches as outlined in Fig. 1 [changes ① and ②]. Keeping in mind the end goal to represent the additions of the two changes with a commonsense case, Fig. 3 shows the conduction misfortunes of a business MOSFET with low RdsON as a component of obligation cycle for the voltage polarization bend of a business hydrogen Fuel Cell. It can be seen that the aggregate conduction misfortunes un-der stage move ZVS [+ bend that incorporates flowing current] are significantly higher than misfortunes just connected with influence exchanged to the auxiliary. The misfortunes have been figured utilizing the rms estimation of the current through switchM1 and the MOSFET ON-resistance RdsON , which is an element of the gadget temperature

$$P_{LossCon} = R_{Dson} i_{M1}^2 \quad (a)$$

For instance, the IRFB4110 has 3.7 mΩ at 250 C and 6 mΩ at 1000 C [run of the mill], bringing about 35 W conduction misfortunes under 75 A rms at 1000 C. At the point when the exchanging misfortunes are broke down, a similar influence gadget encounters under 6.5 W amid the turn-ON move because of its yield capacitance Coss when exchanging at 40 kHz with vFuel Cell = 22 V as given in the accompanying:

$$P_{LossCon} = ([1/2]C_{oss}F_{sw}V_{FC}^2) \quad (b)$$

Hence, it can be gathered that in this specific low-voltage high-current application, the productivity pick up coming about because of diminishing flowing current in four switches exceeds those of exchanging misfortunes, particularly under substantial stacking conditions. At the point when the lower switches are viewed as, the situation is considerably more great, as M2 and M4 advantage from bring down conduction misfortunes, as well as work in ZVS because of the change ③in the regulation [+50% obligation cycle]. Likewise, the lessening in the conduction interim additionally diminishes copper misfortunes in the transformer windings and favors the utilization of planar attractive with their inborn low spillage inductance to expand influence exchange.

B. Yield Rectifier Phase

The yield rectifiers add to control misfortunes because of conduction and switch recuperation. Since the yield voltage of the power converter is high (i.e., 220 V to supply a solitary stage inverter), the conduction current is normally a couple of amperes for every kilowatt of yield control (i.e., 4.54 A), making the turn around recuperation misfortunes the predominant element. Switch recuperation charge is a component of the forward conduction current (IF) and the rate of progress of current (di/dt), and also working temperature of the gadget. The invert recuperation misfortunes can be assessed by utilizing the recuperation charge, exchanging recurrence (Fsw), and switch connected voltage (VR), including the pinnacle ringing an incentive as takes after:

$$P_{Loss} = Q_{rr}V_{r}F_{sw} \quad (c)$$

As a straightforward audit of this joined impacts, a calculated relationship among di/dt, the IF , and Qrr in which the underlying forward current is given by IF 3 > IF 2 > IF 1. As demonstrated in [3] the turn around recuperation misfortunes can be lessened by methods for controlling di/dt [design objective [c]] and by decreasing the invert top voltage VR delivered by transformer motions [design objective [d]]. For this reason, the Lzvs inductor is reflected to the auxiliary and put at the yield of every upper rectifier D5 and D7 [change ③]. This procedure restrains the di/dt in the upper rectifiers, takes out turn around recuperation in the lower diodes D6 and D8, and decreases fundamentally the transformer motions by keeping a zero-voltage state at the optional.



As will be seen, the procedure keeps away from concurrent conduction of D5 , D6 , D7 , and D8 , in this manner decreasing undesirable ringing that happens when the essential current matches the inductor yield current, which brings about an extreme voltage venture in the auxiliary that makes ringing, and along these lines, electromagnetic impedance. In the accompanying area, the operation of the full-connect forward converter and the impact of the proposed adjustments for proficiency upgrades are displayed in detail finished the different exchanging interims.

IV. PROCEDURE INTERMISSION AND LOSS-DIMINUTION RESULTS

The blend of the proposed systems, Lzvs inductor reflection to the yield of the rectifier (①), right-adjusted entryway signals for the upper switches (②), and +50% obligation cycle in the lower switches (③) are researched in detail in this area. The exchanging arrangement for MOSFETs M1, M2, M3, and M4 alongside the primary waveforms for the systems under examination. Move interims have been misrepresented for lucidity.

A. MOSFETs Waveform and Its Brief Manipulations

The waveforms for MOSFETs M1 and M4 and their particular body diodes D1 and D4 are appeared amid a full-cycle period, including the door signals G1 and G4, deplete to-source voltages vM1 and vM4 , streams for the MOSFETs n-channel iM1 and iM4 , and the body diodes iD1 and iD4. As can be seen, not at all like stage move ZVS or full converters, the proposed procedures avert superfluous coursing current in the transformer and through the MOSFETs, and permits control exchange amid the conduction interim.

This is a key necessity in low-voltage, high-current applications, where the conduction misfortunes are significant and exceed exchanging misfortunes at direct exchanging frequencies. Too, the +50% obligation cycle regulation succession guarantees zero-voltage moves in MOSFETs M2 and M4. The increases depicted in this segment are additionally upgraded in the yield rectifier as portrayed in the accompanying segment.

B. Resulting Waveforms of Rectifier

So as to finish the examination of the waveforms and productivity picks up, the yield rectifier ought to be explored. The current and voltage waveforms for D7 (upper) and D8 (lower) diodes are exhibited in Fig. 8, where both conduction misfortunes and turn around recuperation moments can be recognized. In rundown, the waveforms for the proposed delicate exchanging methods uncover the accompanying changes.

(A) The assistant inductors La and Lb shape the present waveforms of D5 and D7 amid invert recuperation. Consequently, the inductor esteems can be chosen to accomplish a coveted Qrr in the upper diodes and, thus, control the aggregate turn around recuperation control misfortunes.

(B) Diodes D6 and D8 encounter irrelevant invert recuperation misfortunes, not at all like the stage move ZVS topology, which is ex plained by close to zero forward current when the decreased turn around voltage is connected.

(C) The nearness of La and Lb diminish motions and the pinnacle switch voltage connected to D6 and D8 that outcome from transformer ringing.

Transformer swaying brings about undesirable impact, for example, high most extreme invert voltage rating for the diodes, EMI, over voltage amongst windings, and power misfortunes in assistant snubber circuits. The idea of keeping away from a zero-voltage condition on the transformer optional is tended to by forestalling concurrent conduction of D5 , D6 , D7 , and D8 . Subsequently, the turn-ON beat is incompletely reflected to the optional of the transformer as though the converter were working in broken conduction mode. Subsequently, the motions are diminished under any stacking condition.

C. Regularity Reply and Active Performance

The recurrence reaction of the control-to-yield normal for the full-connect topology, which is a buck-inferred topology, is commanded by the exchange capacity of the yield channel [L and When the converter is worked in stage move ZVS, an arrangement inductance is required to restrict the present rate of progress in the essential to create delicate moves in the switches [24]. This restriction, diminishes the powerful obligation cycle reflected to the auxiliary, along these lines, influencing the control-to-yield trademark. Subsequently, a manufactured dumping impact is made in the recurrence reaction by the arrangement inductance, which mollifies the control-to-yield trademark top at the thunderous recurrence of the channel [25]. In shut circle operation utilizing conventional pay [little flag], the manufactured dumping does not have any detectable impact in stage and pick up edges.

A comparative conduct is experienced when the proposed strategies are utilized utilizing conventional compensators, in this way, demonstrating a dynamic reaction like that of a stage move ZVS. In this investigation, keeping in mind the end goal to encourage the proficiency assessment prepare, numerous estimations were performed with a shut circle controller [little flag] in relentless state operation. The controller was acknowledged with an internal current circle [inductor current] and an external voltage circle. Approval of the waveforms and similar proficiency estimations are displayed in the accompanying segment.

V. SIMULATION RESULTS

TABLE I Converter Parameters

Input Parameters	Assessment Boundaries
v _{fc}	18-40V
v _o	220V
L	1.33mH
D _a , L _b	10uH
C	680uF
C _i	4400uF
F _{sw}	40-100kHz
T/f primary turns N _p	2
T/f secondary turns N _s	26



The below figure 2 shows the Upper side MOSFET M1 waveforms in the proposed modified topology under medium loading condition: drain-to-source voltage (Ch1), gate-to-source signal (Ch2), and transformer-secondary current (Ch4).

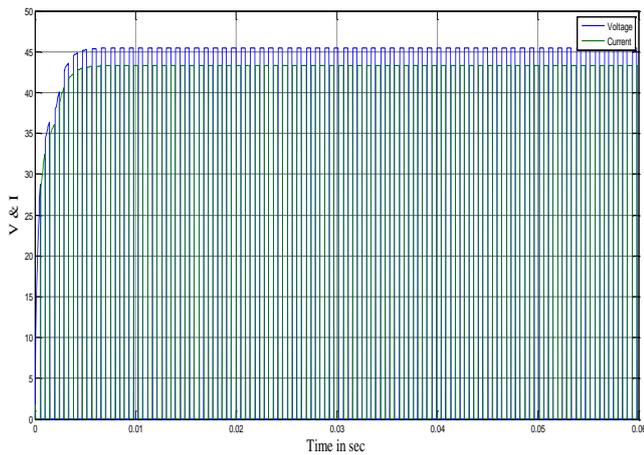


Fig. 2. Upper side MOSFET M1 waveforms in the proposed modified topology under medium loading condition: drain-to-source voltage (Ch1), gate-to-source signal (Ch2), and transformer-secondary current (Ch4).

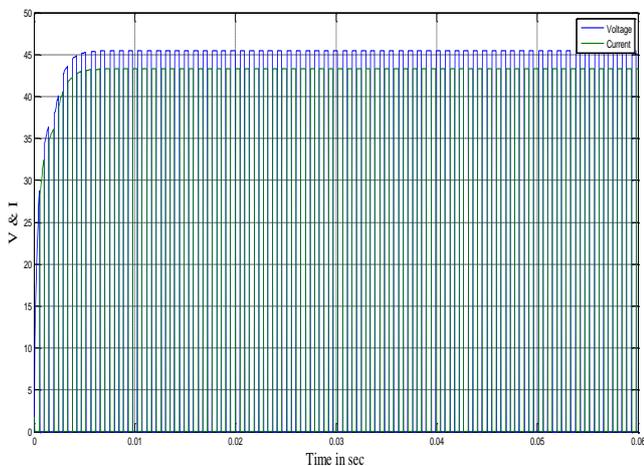


Fig.3. Lower side MOSFET M4 waveforms in the proposed modified topology under medium loading condition: drain-to-source voltage and current (Ch4).

Concentrating on the rectifier organize, the upper yield rectifier D7 waveforms with the proposed procedures are appeared in Fig.5. The kill move from forward-one-sided to blocking is shown in interim T1 . The impact of Lb and Llk can be found in the present move, bringing about direct switch recuperation misfortunes toward the start of T2 . The finish of the interim T7 compares to the moment when the current in Lb coordinates the current in the yield channel inductor L. Amid T8 , the slant of i_{D7} is for the most part because of L. The conduction interim is characterized from T7 to T1 of the following exchanging cycle. As can be seen, the transformer wavering are little and experience a quick damping start at T2 [no snubber have been incorporated into the model]. Just an underlying pinnacle is experienced because of the impact of the stray inductance in the present way [lobby impact sensor estimation way] and Lb. This gives an unmistakable sign that the proposed course of action just requires a little nearby snubber associated from

D7 cathode to L include terminal, instead of the notable massive snubber circuit in ZVS circuits.

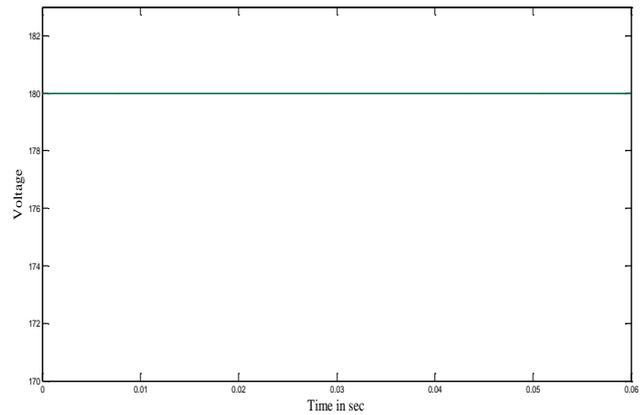


Fig.4. Upper Side Diode Medium Loading Condition.

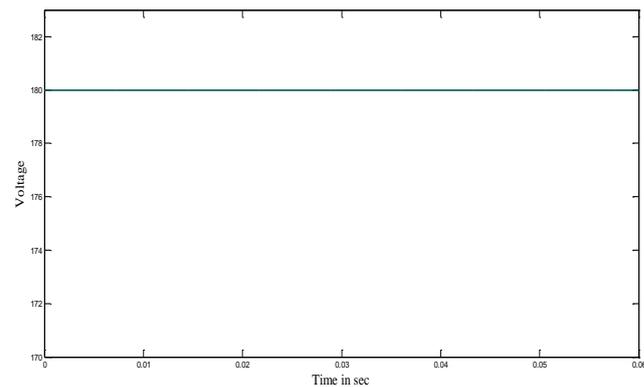


Fig.5. Upper side diode D8 waveforms in the proposed modified topology under medium loading condition.

The change that outcomes from the proposed alterations is better refreshing in the exploratory waveforms for D8 portrayed in above figures. Because of the interleaving impact of La and Lb amid T3–T5 interim, diode D8 encounters a quick move from high conduction current to almost zero current. Toward the start of T7, the converter input voltage is somewhat reflected to the auxiliary and squares D8 promptly with a move that produces unimportant switch recuperation misfortunes in D8. Also, the blocking move presents direct ringing toward the start of T7 while the upper diode current i_{D7} increase. At the point when this is contrasted with the conduct under stage move ZVS, which is displayed in circuit design, diode D8 presents undesirable switch recuperation misfortunes toward the start of interim T8 , where a little negative-current pinnacle can be seen because of the impact of Q_{rr} . As anticipated by the investigation, the ringing top voltage in D8 is high, expanding the invert recuperation misfortunes and requiring a cumbersome snubber. At long last, to check that the info current is sure, a basic prerequisite in FC control change, Above figures exhibits the information current of the converter and the transformer input voltage working under medium stacking condition. As anticipated by the examination, the present stays positive amid all the exchanging interims.

A. Comparative Efficiency Measurements

The consolidated exchanging and conduction misfortunes for the proposed delicate exchanging procedures are exhibited in this area. A stage move ZVS is utilized as a source of perspective topology for near assessment.

A similar power gadgets, control transformer, drivers, dead-time addition, heatsink and fan, and yield channel were utilized in both cases to guarantee a reasonable examination [see Table I]. Note that the target of the exploratory effectiveness estimations is to represent the proficiency picks up with the proposed changes as opposed to playing out a flat out estimation of the converter productivity. The proficiency estimation represents the power switches, printed circuit board, associations, and attractive parts and does exclude misfortunes in the controller and drivers. For ZVS operation, the helper Lzvt inductor and snubbers were incorporated, while expelling La and Lb .

A few tests were performed for different information voltages $v_{fc} = 18, 25, \text{ and } 30 \text{ V}$ under factor stacking conditions [50–1000 W extend] for both power converters. The outcomes are appeared in above figures, delineating the productivity as an element of yield power and info voltage in a 3-D plot. It is vital to highlight that despite the fact that effectiveness portrayal in control converters is customarily performed utilizing settled info voltage, FC control transformation requires the utilization of a polarization bend [variable contribution] to represent the remiss voltage direction that is trademark in these power sources. In this way, a surface effectiveness estimation gives a superior intends to correlation, as displayed in above figure.

The productivity profile accomplished with the proposed delicate exchanging strategies, alluded to as Modified in the figure is delineated with circle markers, while the stage move ZVS is outlined with star markers. It can be seen that the proposed alterations show a noteworthy effectiveness increase under any working condition. For instance, a proficiency pick up of 3%–4% in a power converter with a general productivity of 90% gives a change near 30%–40% in the warm administration of the power organize and permits the utilization of lower cost control semiconductors/Heatsinks.

This can be considered as a magnificent change toward control thickness and cost of the power transformation organize, while keeping up the straightforwardness of a full-connect topology. Too, the productivity picks up result in total fuel reserve funds [i.e., hydrogen or methanol] under any working condition [light, medium, and substantial] by utilizing the proposed delicate exchanging procedures.

VI. EXPERIMENTAL RESULTS



Fig.6. Experimental Setup View

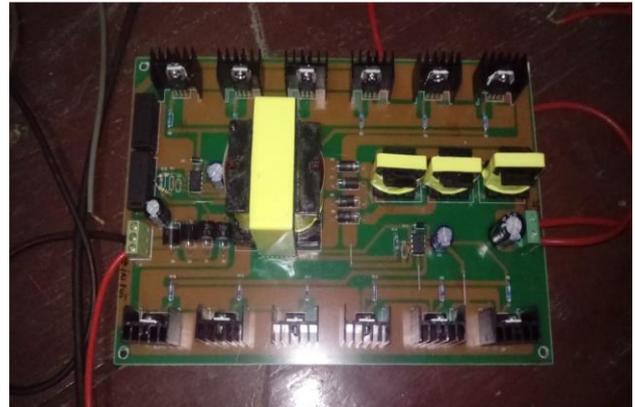


Fig.7. Circuit Designing Nature



Fig.8. Reading Analysis



Fig.9. Oscilloscope Resulting View

VII. CONCLUSION

This paper defines minimization of conduction losses using a fuzzy based controller for new converter topology. It will improve transformation productivity and voltage direction. The transformer used to decrease weight on diodes in rectifier and to limit the coursing streams.



REFERENCES

1. J. E. Larminie and A. Dicks, Fuel Cell Systems Explained. Chichester, U.K.: Wiley, 2000.
2. M. Ordonez, P. Pickup, J. E. Quaioco, and M. T. Iqbal, "Electrical dynamic response of a direct methanol fuel cell," IEEE Power Electron. Soc. Newslett., vol. 19, no. 1, pp. 10–15, Jan. 2007.
3. J. Wang, F. Z. Peng, J. Anderson, A. Joseph, and R. Buffenbarger, "Low cost fuel cell converter system for residential power generation," IEEE Trans. Power Electron., vol. 19, no. 5, pp. 1315–1322, Sep. 2004.
4. J. Wang, M. Reinhard, F. Z. Peng, and Z. Qian, "Design guideline of the isolated DC-DC converter in green power applications," in Proc. IEEE Power Electron. Motion Control Conf., 2004, vol. 3, pp. 1756–1761.
5. R. Gopinath, S. Kim, J. Hahn, P. N. Enjeti, M. B. Yeary, and J.W. Howze, "Development of a low cost fuel cell inverter system with DSP control," IEEE Trans. Power Electron., vol. 19, no. 5, pp. 1256–1262, Sep. 2004.
6. L. Palma and P. N. Enjeti, "A modular fuel cell, modular DC-DC converter concept for high performance and enhanced reliability," IEEE Trans. Power Electron., vol. 24, no. 6, pp. 1437–1443, Jun. 2009.
7. G. Holmes, P. Atmur, C. C. Beckett, M. P. Bull, W. Y. Kong, W. J. Luo, D. K. C. Ng, N. Sachchithanathan, P. W. Su, D. P. Ware, and P. Wrzos, "An innovative, efficient current-fed push-pull grid connectable inverter for distributed generation systems," in Proc. IEEE Power Electron. Spec. Conf., 2006, pp. 1504–1510.
8. E.-H. Kim and B.-H. Kwon, "High step-up resonant push-pull converter with high efficiency," IET Power Electron., vol. 2, no. 1, pp. 79–89, 2009.
9. S. Jung, Y. Bae, S. Choi, and H. Kim, "A lowcost utility interactive inverter for residential fuel cell generation," IEEE Trans. Power Electron., vol. 22, no. 6, pp. 2293–2298, Nov. 2007.
10. H. Kim, C. Yoon, and S. Choi, "A three-phase zero-voltage and zerocurrent switching DC-DC converter for fuel cell applications," IEEE Trans. Power Electron., vol. 25, no. 2, pp. 391–398, Feb. 2010.
11. J. Mason, D. J. Tschirhart, and P. K. Jain, "New ZVS phase shift modulated full-bridge converter topologies with adaptive energy storage for SOFC application," IEEE Trans. Power Electron., vol. 23, no. 1, pp. 332–342, Jan. 2008.
12. X. Kong and A. M. Khambadkone, "Analysis and implementation of a high efficiency, interleaved current-fed full bridge converter for fuel cell system," IEEE Trans. Power Electron., vol. 22, no. 2, pp. 543–550, Mar. 2007.
13. H. Cha and P. Enjeti, "A novel three-phase high power current-fed DC/DC converter with active clamp for fuel cells," in Proc. IEEE Power Electron. Spec. Conf., 2007, pp. 2485–2489.
14. Averbeg, K. R. Meyer, and A. Mertens, "Current-Fed Full Bridge Converter for Fuel Cell Systems," in Proc. IEEE Power Electron. Spec. Conf., 2008, pp. 866–872.
15. M. Nymand and M. A. E. Andersen, "High-efficiency isolated boost DCDC converter for high-power low-voltage fuel-cell applications," IEEE Trans. Ind. Electron., vol. 57, no. 2, pp. 505–514, Feb. 2010.
16. J.-M. Kwon, E.-H. Kim, B.-H. Kwon, and K.-H. Nam, "High-efficiency fuel cell power conditioning system with input current ripple reduction," IEEE Trans. Ind. Electron., vol. 56, no. 3, pp. 826–834, Mar. 2009.
17. M. H. Todorovic, L. Palma, and P. N. Enjeti, "Design of a wide input range DC-DC converter with a robust power control scheme suitable for fuel cell power conversion," IEEE Trans. Ind. Electron., vol. 55, no. 3, pp. 1247–1255, Mar. 2008.
18. R. L. Andersen and I. Barbi, "A three-phase current-fed push-pull DC-DC converter," IEEE Trans. Power Electron., vol. 24, no. 2, pp. 358–368, Feb. 2009.
19. J.-M. Kwon and B.-H. Kwon, "High step-up active-clamp converter with input-current doubler and output-voltage doubler for fuel cell power systems," IEEE Trans. Power Electron., vol. 24, no. 1, pp. 108–115, Jan. 2009.
20. Y. Lembeye, V. D. Bang, G. Lefevre, and J.-P. Ferrieux, "Novel halfbridge inductive DC-DC isolated converters for fuel cell applications," IEEE Trans. Energy Convers., vol. 24, no. 1, pp. 203–210, Mar. 2009.