Improvement of Power System Transient Stability Using an Intelligent Control Method

Mohsen Darabian, Bahram Khorram, Mehdi Azari

Abstract—Shunt Flexible AC Transmission System (FACTS) devices, when placed at the mid-point of a long transmission line, play an important role in controlling the reactive power flow to the power network and hence both the system voltage fluctuations and transient stability. In this paper, a new intelligent controller used to control the output of an SVC to damp power system oscillations is developed. This controller is an online trained wavelet neural network controller (OTWNNC) with adaptive learning rates derived by the Lyapunov stability. Effectiveness of the proposed technique is robustness to different operating conditions and disturbances. The effectiveness of the proposed controllers is demonstrated on an 2-machine system. Results obtained show improvement in the overall system damping characteristics using the proposed method (OTWNNC).

I. INTRODUCTION

Power system stability (PSS) control is an important task in PSS operation [1]. Several factors, such as external disturbances or internal mechanical torques, may easily affect system stability. With the development of power electronics, the structural control of electric power networks has recently attracted more attention. In this context, flexible AC transmission system (FACTS) devices are becoming more popular. Due to their fast response, these devices are used to dynamically adjust the network configuration to enhance steady-stat performance as well as dynamic stability [2]–[5]. The availability of FACTS devices, such as thyristor controlled series compensators (TCSCs), static var compensators (SVCs), and static synchronous series compensators (SSSCs), can provide variable turn and/or series compensation [3]. However, these devices can interfere with one another. When the controller parameters of a dynamic device are tuned to obtain the best performance, control conflicts that arise between various FACTS controllers may lead to the onset of oscillations [3, Ch. 9]. Thus, the coordinated control of these devices is very important [4]. TCSCs and SVCs have been widely studied in the technical literature and have been shown to significantly enhance system stability [6]–[8]. Therefore, this paper employs these two devices and proposes a new coordinated control scheme to enhance the dynamic response of a multi-machine PSS.

Different FACTS device control methods have been proposed for power oscillation damping and transient stability improvement [9]. One popular damping control method uses a washout filter followed by a th order lead-lag controller [10]–[14]. In general, the parameters of a lead-lag controller are designed using the pole-zero location method [11], [12], [14]. Modern PSs are large-scale and complex. Disturbances typically change the network topology and result in a nonlinear response. Therefore, capabilities of traditional control laws based on linearized models are limited. To address this problem, FACTS control using fuzzy control scheme has been proposed [7–16]. Unlike previous control configurations, this paper proposes a fuzzy lead-lag control scheme for the control and coordination of TCSC and SVC devices in a multi-machine PS. In this new control configuration, an FC is designed to adaptively adjust the parameters of lead-lag controllers at each control time step. The performance advantage of the FACTS devices equipped with the fuzzy lead-lag controller is verified through comparison with traditional lead-lag controllers. Based on aforementioned before, a novel technique is very essential for the stabilization of power systems. Inspired algorithms such as Genetic Algorithm (GA) [17,18], Bacterial Foraging Optimization (BFO) [19] Artificial Bee Colony (ABC) algorithm [20] and Tabu Search (TS) [21] algorithm especially with stochastic search techniques have been employed to find optimal value of PSS stabilizer parameters. Recently, SO algorithm has become available and a promising technique for real world optimization problems. PSO as a population (swarm) based algorithms can solve a variety of difficulties associated with optimization problems. PSO applied to better stability of the power system [22, 23,24,25,26]. In this paper is the application of an online trained wavelet neural network controller to provide the necessary control signal to the SVC so that power system oscillations are quickly damped out, since the Lyapunov stability method is used to guarantee the convergence of proposed controller, the overall control system is globally stable and hence, the transient stability of power system is improved; the control error can be reduced to zero by selecting appropriate parameters and learning rates; and the proposed controller can achieve favorable controlling performance. Meanwhile, no neural network identifier is used to approximate the dynamic of controlled power system.

This paper is set out as follows: System model in Section II Problem statement is formulated in Section III. Heuristic optimization methods for solving the problem are presented in Section III. The application of the proposed model and simulation results are presented in Section V and finally, the conclusion is presented in Section VI.

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II. SYSTEM MODEL

A. Power System Model

Fig. 1 shows a single-line diagram of the studied system consisting of two machines and one large load center at bus3. The generation capacity of first power generation substation (G1) is 1000 MVA. The capacity of other one (G2) is 5000MVA. A large load is used to model the load center of approximately 6000MW. Both L1 and L2 are 350-km long. The SVC (400-MVAR) is placed at the generator bus 2 to provide instantaneous reactive power modulation for voltage maintenance. The system data are given in the Table 1 and Table 2. See Appendix A.

B. SVC Structure

SVC is basically a shunt connected static var generator/load whose output is adjusted to exchange capacitive or inductive current so as to maintain or control specific power system variables: typically, the controlled variable is the SVC bus voltage. One of the major reasons for installing a SVC is to improve dynamic voltage control and thus increase system load ability. An additional stabilizing signal, and supplementary control, superimposed on the voltage control loop of a SVC can provide damping of system oscillation as discussed in [27-28].

![Fig1: Power system under study](image)

Table 1: The parameters used for G1 and G2

<table>
<thead>
<tr>
<th>Parameters</th>
<th>Value</th>
<th>Parameters</th>
<th>Value</th>
</tr>
</thead>
<tbody>
<tr>
<td>$V_{L1}$</td>
<td>13.8kv</td>
<td>$x_q$</td>
<td>0.50p.u</td>
</tr>
<tr>
<td>$f$</td>
<td>60HZ</td>
<td>$x_q'$</td>
<td>0.243p.u</td>
</tr>
<tr>
<td>$r_a$</td>
<td>0.003p.u</td>
<td>$x_l$</td>
<td>0.18p.u</td>
</tr>
<tr>
<td>$x_d$</td>
<td>1.305p.u</td>
<td>$T_{do}$</td>
<td>1.01s</td>
</tr>
<tr>
<td>$x_d'$</td>
<td>0.296p.u</td>
<td>$T_{do}'$</td>
<td>0.053s</td>
</tr>
<tr>
<td>$x_{d''}$</td>
<td>0.252p.u</td>
<td>$T_{qo}$</td>
<td>0.1s</td>
</tr>
<tr>
<td>$x_q''$</td>
<td>0.474p.u</td>
<td>$H$</td>
<td>3.7</td>
</tr>
</tbody>
</table>

Table 2: Parameters used for the excitation system

<table>
<thead>
<tr>
<th>Parameters</th>
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<th>Parameters</th>
<th>Value</th>
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<tbody>
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<td>$k_l$</td>
<td>0.001p.u</td>
</tr>
<tr>
<td>$T_a$</td>
<td>0.001s</td>
<td>$T_l$</td>
<td>0.1s</td>
</tr>
<tr>
<td>$k_e$</td>
<td>1p.u</td>
<td>$E_{fmin}$</td>
<td>-5p.u</td>
</tr>
<tr>
<td>$T_e$</td>
<td>0s</td>
<td>$E_{fmax}$</td>
<td>5p.u</td>
</tr>
</tbody>
</table>

III. PROPOSED METHOD

A. Online trained wavelet neural network controller (OTWNNC)

The proposed OTWNNC is shown in Fig.2. according to Fig.2, the smart control system contains an online trained wavelet neural network controller. Also, computing block the active power transferred through the line L1 is obtained. The active Power output of the block is compared with a reference value $P_{ref}$. In fact, this reference value is equal to the active power transferred via L1 in steady-state of power system.

According to figure 2, this error can be used as input WNN. Finally, the output of this intelligent control system $u$ is added to the reference voltage of SVC ($V_{ref}$). In order to determine the SVC susceptance $B_{eq}$ for the maintaining voltage of voltage regulator is used (difference between the measured voltage $V_m$ and the reference voltage $(V_{ref}+u)$). Therefore, the SVC regulates its output voltage based on the summation of the reference voltage and the output of the intelligent control system.
The proposed wavelet neural network model training algorithm is described as the calculation of a gradient vector in which each component in the training algorithm is defined as the derivative of a cost function with respect to parameters of WNN controller so that the cost function is minimized. Hence, the chain rule is used and the general method is referred as the back error propagation learning rule, since the gradient vector is computed in the direction opposite to the flow of the output of each node. The cost function is expressed by equation 3:

\[ E = \frac{1}{2} e^2 = \frac{1}{2} (P_{\text{ref}} - P)^2 \]  

(3)

According to general back-propagation algorithm [29], For the output layer, the error term to be propagated is computed as follows:

\[ \delta_\theta = -\frac{\partial E}{\partial u} = \left[ -\frac{\partial E}{\partial \delta} \right]_u = \frac{\partial E}{\partial P} \frac{\partial P}{\partial \delta} \frac{\partial \delta}{\partial u} \]  

(4)

Then update \( W_j(k) \) by using \( W_j(k+1) \) in backward computation of the WNN the following equation (5):

\[ w_j(k+1) = w_j + \eta_w \frac{\partial E}{\partial w_j} = w_j + \eta_w \delta_\theta \phi_j \]  

(5)

According to equation (5), \( \eta_w \) and \( k \) are the learning rate of the weight and the number of iteration. Since there is one neuron in the output layer, only the error term must be computed and propagated. So let this be equation (6):

\[ \delta_i = -\frac{\partial E}{\partial \text{net}_j} = \left[ -\frac{\partial E}{\partial u} \right]_{\phi_j} = \delta_\theta w_j \text{net}_j - 1 \]  

exp\(-0.5\text{net}_j^2\)  

(6)

Also, update \( m_{ij} \) and \( d_{ij} \) are expressed by equation (7) and (8).

\[ \Delta m_{ij} = -\eta_m \frac{\partial E}{\partial m_{ij}} = -\eta_m \frac{\partial E}{\partial \delta} \frac{\partial \delta}{\partial \phi_j} \frac{\partial \phi_j}{\partial \text{net}_j} \frac{\partial \text{net}_j}{\partial m_{ij}} \]  

\[ = -\eta_m \delta_i \]  

(7)

\[ \Delta d_{ij} = -\eta_d \frac{\partial E}{\partial d_{ij}} = -\eta_d \frac{\partial E}{\partial \phi_j} \frac{\partial \phi_j}{\partial \text{net}_j} \frac{\partial \text{net}_j}{\partial d_{ij}} \]  

\[ = -\eta_d \delta_i \]  

(8)

Finally, translation and dilation of the wavelet layer can be updated according to the following equations(9) and (10):

\[ m_{ij}(k+1) = m_{ij}(k) + \Delta m_{ij} \]  

(9)

\[ d_{ij}(k+1) = d_{ij}(k) + \Delta d_{ij} \]  

(10)

According to above equations \( \eta_m \) and \( \eta_d \) denote the learning rates of the translation and dilation of the wavelet layer. As regards, the sensitivity of the system \( \frac{\partial E}{\partial u} \) cannot exactly be calculated, an identifier must be implemented to compute the sensitivity of the power system. So at this point to increase the speed of the on-line training, the following equation is used (11):

\[ \delta_\theta \equiv e + e(1 - z^{-1}) \]  

(11)
We now analyze the convergence of the proposed identifier and controller. The convergence of the WNN is related to select the appropriate learning rate. Since the learning rate is an essential factor for determining the performance of the neuro identifier and the neuro controller trained via the back propagation (BP) or gradient descent (GD) method, it is important to find the optimal learning rate [30]. However, in the conventional GD method, it is difficult to choose an appropriate learning rate because the learning rate is usually selected as a time invariant constant by trial and error. Accordingly, the ALRs, which can adapt rapidly the change of the plant, have been researched for the various neural networks [31,32,33]. Based on this progress about the ALRs, we devise some theorems for the convergence of the proposed indirect adaptive control system.

D.1. Convergence analysis for identification

Let us define a discrete Lyapunov function as:

\[ V(k) = E(k) = \frac{1}{2} e^T(k) e(k) \]  
(12)

where \( e(k) \) is the identification error. The change in the Lyapunov function is obtained by equation (13):

\[ \Delta V(k) = V(k + 1) - V(k) = \frac{1}{2} e^T(k + 1) - e^2(k) \]  
(13)

The error difference can be represented by equation (14):

\[ \Delta e(k) = e(k + 1) - e(k) = [\frac{\partial e(k)}{\partial W_i}] \Delta W_i \]  
(14)

where \( W_i \) is an arbitrary component of the vector \( W \) of the WNN and is equal to (15):

\[ W = [w, m, d]^T \]  
(15)

And the corresponding change of \( W_i \) is denoted by \( \Delta W_i \) as:

\[ \Delta W_i = \eta_w \delta \frac{\partial u}{\partial W_i} \]  
(16)

Where \( \eta_w \) is an arbitrary diagonal element of the learning rate matrix \( \eta \) corresponding to the weight component \( W_i \).

Proposition 1. Let \( \eta = diag[\eta_1, \eta_2, \eta_3] = diag[\eta_1, \eta_2, \eta_3] \) be the learning rates for the weights of the WNN and define \( C_{max} \) as:

\[ C_{max} = [c_{max}^1, c_{max}^2, c_{max}^3]^T = \left[ \max \| \frac{\partial u}{\partial W} \|, \max \| \frac{\partial u}{\partial m} \|, \max \| \frac{\partial u}{\partial d} \| \right]^T \]  
(17)

In the above equation \( \| \| \) denotes the Euclidean norm and the convergence is guaranteed if \( \eta \) is chosen to satisfy

\[ \eta_w = \lambda / C_{max} \]  
(18)

where \( \lambda \) is a positive constant gain. Full details are given in appendix B.

Proposition 2. Let \( \eta_w \) be the learning rate for weights \( w \). The convergence of WNN will then be guaranteed if the following learning rate is used:

\[ \eta_w = \lambda / N_w \]  
(19)

In the above equation \( N_w \) is the neurons number of the wavelet layer. Full details are given in appendix C.

In order to prove Proposition 3, the following lemmas are used.

Lemma 1. Let \( f(t) = t \exp(-t^2) \). Then \( |f(t)| \leq \sqrt{\pi} t \in \mathbb{R} \).

Lemma 2. Let \( g(t) = t \exp(-t^2) \). Then \( |g(t)| \leq \sqrt{\pi} t \in \mathbb{R} \).

Proposition 3. Let \( \eta_w \) and \( \eta_d \) be the learning rates of the translation, and dilation, respectively. The convergence of WNN will then be guaranteed if the following equations are used (19) and (20). The following equations \( N_i, [w]_{max} \) and \( |d|_{min} \) are the input number of the WNN, the maximum of the absolute value of weights vector and the minimum of the absolute value of dilations vector, respectively. Full details are given in appendix D.

\[ \eta_w = \eta_w \left[ \frac{|d|_{min}}{2|w|_{max} \exp(-0.5)} \right]^2 \]  
(19)

\[ \eta_d = \eta_w \left[ \frac{|d|_{min}}{2|w|_{max} \exp(0.5)} \right]^2 \]  
(20)

IV. RESULTS AND SIMULATIONS

To investigate the performance of the proposed controller, the two-machine power system shown in Fig.2. To show the robustness of the proposed design approach, different operating conditions and contingencies are considered for the system with and without controller. Hence, different loading conditions given in Table 3 are considered. Two different operating conditions (nominal and heavy) are considered and simulation studies are carried out under different fault disturbances and fault clearing sequences. The effectiveness of the performance of the proposed method our trial and error studies show that the controller performance is often similar for sampling rates in the range of (30–100) Hz. Therefore, a sampling frequency of 60 Hz is used in these studies. Further details of the proposed method (OTWNNC) is shown in Table 4.

<table>
<thead>
<tr>
<th>Loading conditions</th>
<th>G1[p.u]</th>
<th>G2[p.u]</th>
</tr>
</thead>
<tbody>
<tr>
<td>Nominal Loading</td>
<td>0.95</td>
<td>0.81</td>
</tr>
<tr>
<td>Heavy Loading</td>
<td>1</td>
<td>0.99</td>
</tr>
</tbody>
</table>

Table3: Different loading conditions.

<table>
<thead>
<tr>
<th>Number of existing neurons</th>
<th>Input layer(N_i)</th>
<th>Wavelet layer(N_w)</th>
<th>Output layer</th>
</tr>
</thead>
<tbody>
<tr>
<td>OTWNN</td>
<td>2</td>
<td>10</td>
<td>1</td>
</tr>
</tbody>
</table>

Table4: The structure of OTWNNC for the simulations.

Case 1: Nominal loading condition, one-phase to ground and three-phase to ground fault

The behavior of the proposed controllers is verified at nominal loading condition under two disturbances. In the first case, a one-phase to ground (L–G) fault is applied at the bus2 at \( t = 1.1s \) and cleared at \( t = 1.24s \). Fig4-a show the response of \( \Delta W_{12} \) due to this disturbance for light loading condition. According to figure 4-a capability of the proposed coordinated controller in reducing the settling time and damping power system oscillations. Moreover, the settling time of these oscillations is \( T_s = 2.81s \) for proposed method (OTWNNC). So the proposed controller is capable of providing sufficient damping to the system oscillatory modes compared with no controller. Fig 4-b shows the generator rotor angle changes. In the second case, a three-phase to ground (L–L–L–G) fault is applied at the bus1 at \( t = 1.1s \) and cleared at \( t = 1.2s \) Fig5-a. It is clear that the performance of proposed controller in damping the oscillations is acceptable. Also, the settling time of these oscillations is \( T_s = 3.26s \) for proposed method (OTWNNC). It can be seen from Fig. 5-b that the first swing in the rotor angle is reduced to \( \delta = 52.76 \) (with proposed control). Also, the output of OTWNNC and the adaptive learning rates for the three-phase to ground fault are illustrated in Fig. 6.
The effectiveness of the proposed controllers is also examined at heavy loading condition. In the first case, it is assumed that an L–L–G fault is occurred at bus 3 during 100 ms. The system speed deviation and power angle response under this contingency is shown in Fig. 7a and b, which clearly depicts the robustness of proposed controllers for changes in operating condition and fault location. According to Fig7-a, the settling time of these oscillations is $T_s = 2.73s$ for proposed method (OTWNNC). There is also the power angle is reduced to $\delta = 53.11$ Fig 7-b.

In the second case, a three-phase (L-L-L) to ground is considered at bus 3 during 140 ms. Fig.8a and b shows the system response for the following contingency. It is clear from the figures that the proposed controller is robust and provides efficient damping even under heavy disturbance conditions. Hence, according to figure8-a it is clear from these figures that the proposed controller attains better performance and supplies superior damping compared with the without controller. The required settling time to diminish these oscillations is nearly $3.36 \text{ s}$ for OTWNNC. It can be seen from Fig. 8-b that the first swing in the rotor angle is reduced to $\delta = 52.96$ (with proposed control). Therefore, the designed controller is able to achieve adequate damping to the system oscillatory modes.

**Case 2: Heavy loading condition, two-phase to ground and three-phase to ground fault**
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Case 3: A comparative study

To evaluate the effectiveness and robustness of the proposed Controller in improving the transient stability, the performance of the system with the proposed OTWNN controller is compared to with the results obtained from a lag-lead compensator [34]. As regards, Lag-lead compensators are widely used in power systems for different objectives because of their simple structure and acceptable performance. Fig. 9 shows the lag-lead compensators structure of the power used in the present study. It consists of a gain block with gain Ks, a signal washout block and two-stage phase compensation block. Hence, the signal washout block serves as a high-pass filter, with the time constant Tw, high enough to allow signals associated with oscillations in input signal to pass unchanged. Without it steady changes in input would modify the output. From the viewpoint of the washout function, the value of TW is not critical and may be in the range of 1–20 s [35]. The phase compensation blocks (time constants T1S, T2S and T3S, T4S) provide the appropriate phase-lead characteristics to compensate for the phase lag between input and the output signals. Hence, the difference between Pref and P is chosen as the input of lag-lead compensator. Tw=10 s and T2 =T4 =0.3 s are used in this paper. Also, more efficient methods have been used the controller gain KS and the time constants T1 S and T3 S must be determined. So, the Particle Swarm Optimization (PSO) algorithm is used to determine the optimal parameters of lag-lead compensator. PSO parameters are listed in Table 5.

A. Particle Swarm Optimization:

The PSO is a population based stochastic optimization technique developed by Eberhart and Kennedy in 1995. The PSO algorithm is inspired by social behavior of bird flocking or fish schooling. The system is initialized with a population of random solutions and searches for optima by updating generations. However, unlike GA, PSO has no evolution operators such as crossover and mutation. In PSO, the potential solutions, called particles, fly through the problem space by following the current optimum particles. Compared to GA, the advantages of PSO are that PSO is easy to implement and there are few parameters to adjust. PSO has been successfully applied in many areas. The standard PSO algorithm employs a population of particles. The particles fly through the n-dimensional domain space of the function to be optimized. The state of each particle is represented by its position \( x_i = (x_{i1}, x_{i2}, ..., x_{in}) \) and velocity \( v_i = (v_{i1}, v_{i2}, ..., v_{in}) \), the states of the particles are updated. The three key parameters to PSO are in the velocity update equation (21). First is the momentum component, where the inertial constant \( w \), controls how much the particle remembers its previous velocity [36].
The second component is the cognitive component. Here the acceleration constant C1, controls how much the particle heads toward its personal best position. The third component, referred to as the the social component, draws the particle toward swarm’s best ever position; the acceleration constant C2 controls this tendency. The flow chart of the procedure is shown in Fig 10. Each particle is updated by two “best” values during every iteration. The first one is the position vector of the best solution (fitness) this particle has achieved so far.

\[
v_i^{k+1} = wv_i^k + c_1 r_1 (p_{best} - x_i^k) + c_2 r_2 (g_{best} - x_i^k)
\]

(21)

and

\[
x_i^{k+1} = x_i^k + v_i^{k+1}
\]

(22)

The fitness value \( p_i = (p_{1i}, p_{2i}, ..., p_{mi}) \) is also stored. This position is called phbest. Another “best” position that is tracked by the particle swarm optimizer is the best position, obtained so far, by any particle in the population. This best position is the current global best \( p_g = (p_{1g}, p_{2g}, ..., p_{mg}) \) and is called gbest. At each time step, after finding the two best values, the particle updates its velocity and position according to (21) and (22).

\[
f = \int_0^{t_{sim}} t |w_1 - w_2| dt
\]

(21)

According to figure 11a and b, it is assumed that an L–L–G fault is occurred at bus 2. The system speed deviation and power angle response under this condition are illustrated in Fig 10a-b. It is obvious from the figures that the proposed OTWNN controller demonstrates better damping Properties to low frequency oscillations and faster stability in comparison with without controller. The settling time are Ts = 2.76 and 3.22 s for OTWNNC and Without controller respectively for Fig11-a. Also, it can be seen from Fig. 11-b that the first swing in the rotor angle is reduced from \( d = 37.7^\circ \) (without control) to \( d = 35.9^\circ \) (with proposed control). Consequently, the power transfer ability as well as the power system stability are increased by way of the proposed OTWNN controller. The convergence of PSO is shown in Fig 12.

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**Table 5: Parameters used in PSO algorithm.**

<table>
<thead>
<tr>
<th>Parameters</th>
<th>( N_c )</th>
<th>( c_1 )</th>
<th>( c_2 )</th>
<th>( r_1 )</th>
<th>( r_2 )</th>
</tr>
</thead>
<tbody>
<tr>
<td>Value</td>
<td>200</td>
<td>2</td>
<td>2</td>
<td>1.05</td>
<td>1</td>
</tr>
</tbody>
</table>

**Objective Function:**

In this paper, objective function should be minimized by the PSO algorithm to achieve the optimal parameters. The objective function is expressed by the following equation(21), in this equation W1 and W2 are the rotor speed of M1 and M2; tsim is the time range of simulation. Parameters optimization by PSO algorithms is shown in Table 6.

**Table 6: Final optimal values of parameters of lag-lead compensator.**

<table>
<thead>
<tr>
<th>Optimization Value</th>
<th>Parameters of lag-lead compensator</th>
</tr>
</thead>
<tbody>
<tr>
<td>Value</td>
<td>( k_s ) ( T_{1s} ) ( T_{3s} )</td>
</tr>
<tr>
<td></td>
<td>7.26 0.0451 0.1011</td>
</tr>
</tbody>
</table>
V. CONCLUSIONS

In this study, a new intelligent controller based on wavelet neural network is proposed to control a SVC in order to improve the transient stability in a two-area two-machine power system. In order to achieve the best results for the proposed controller is an online trained wavelet neural network. Using the Lyapunov approach, the convergence theorems for SRWNN have been proven and, from this process, the optimal adaptive learning rates have been established. To further demonstrate the ability of the proposed method, two different loading conditions and with several disturbances are considered. Simulations results assure the effectiveness of the proposed controller in providing good damping characteristic to system oscillations over a wide range of loading conditions and disturbance.

Appendix A

A. Data in Table 1:
ra, the resistance of stator winding of generators; xd, the d-axis synchronous reactance of generators; x'd, the d-axis transient reactance of generators; x'd, the d-axis subtransient reactance of generators; xq, the q-axis synchronous reactance of generators; x'q, the q-axis transient reactance of generators; x'q, the q-axis subtransient reactance of generators; xl, the leakage reactance of generators; T'do, the d-axis transient open-circuit time constant; T'do, the d-axis subtransient open-circuit time constant; T'qo, the q-axis subtransient open-circuit time constant; H, the inertia constant.

B. Data in Table 2:
K, the gain of the first-order system representing the main regulator; Ta, the time constant of the first-order system representing the main regulator; Ke, the gain of the first-order system representing the exciter; Te, the time constant of the first-order system representing the exciter; Kf, the gain of the first-order system representing a derivative feedback; Tf, the time constant of the first-order system representing an adervative feedback; Emax, the upper limit of regulator output; Emin, the lower limit of regulator output.

Appendix B.

From Eq.(12), V(k)> 0. Using Eq.(14), we can obtain:
\[ e(k + 1) = e(k) + \frac{\partial e(k)}{\partial w_l} \Delta w_l \]
\[ e(k + 1) = e(k) - \eta w \frac{\partial e(k)}{\partial w_l} \eta w \frac{\partial e(k)}{\partial w_l} \]
\[ \| e(k + 1) \| = \| e(k) \| \left[ 1 - \eta w \left( \frac{\partial e(k)}{\partial w_l} \right)^T \frac{\partial e(k)}{\partial w_l} \right] \]
\[ \| e(k) \| \left[ 1 - \eta w \left( \frac{\partial e(k)}{\partial w_l} \right)^T \frac{\partial e(k)}{\partial w_l} \right] = \| e(k) \| \gamma \]
Where: \( \gamma = \left[ 1 - \eta w \left( \frac{\partial e(k)}{\partial w_l} \right)^T \frac{\partial e(k)}{\partial w_l} \right] \]
\[ \| e(k) \| \left[ 1 - \eta w \left( \frac{\partial e(k)}{\partial w_l} \right)^T \frac{\partial e(k)}{\partial w_l} \right] = \left[ 1 - \eta w \left( \frac{\partial e(k)}{\partial w_l} \right)^T \frac{\partial e(k)}{\partial w_l} \right] \]
From Eq.(A) and using Eq.(13):
if \[ \left[ 1 - \eta w \left( \frac{\partial e(k)}{\partial w_l} \right)^T \frac{\partial e(k)}{\partial w_l} \right] \leq 1 \] is satisfied, then the convergence of the WNN can be guaranteed. Therefore, we can calculate \( \eta w = \frac{\lambda}{\lambda_{\text{max}}} \).

Appendix C.

C\( ^{1} = \frac{\partial u}{\partial w} = \Phi \), where \( \Phi = [\phi_1, \phi_2, ..., \phi_N] \) is the output vector of the wavelet layer of the WNN. Then, because we have \( \lambda_j \leq 1 \) for all \( j, \| c^{1}(k) \| < 1 \), we can calculate \( \eta w = \frac{\lambda}{\lambda_{\text{max}}} \).

Appendix D.

\[ c^2 = \frac{\partial u}{\partial m_{ij}} = w_j \frac{\partial \phi_j}{\partial m_{ij}} \leq |w_j| \left( \max \left| \frac{\partial \phi_j}{\partial m_{ij}} \right| \right) \]
\[ \leq |w_j| \left( \max \left| \frac{2 \exp (-0.5)}{\left( d_{ij} \right)^2} \cdot \frac{1}{2} \right| \right) \]
Tuse: \( \| c^2 \| < \sqrt{\lambda_{\text{max}}} |w_j| \left( \frac{2 \exp (-0.5)}{|d_{ij}|_{\text{min}}} \right) \)
Then we have:
\[ \eta m = \eta w \left( \frac{|d_{ij}|_{\text{min}}}{2 |w_j| \max \left| \frac{2 \exp (-0.5)}{|d_{ij}|_{\text{min}}} \right|} \right)^2 \]
Since:
\[ c^3 = \frac{\partial u}{\partial d_{ij}} = w_j \frac{\partial \phi_j}{\partial d_{ij}} \leq |w_j| \left( \max \left| \frac{\partial \phi_j}{\partial d_{ij}} \right| \right) \]
\[ \leq |w_j| \left( \max \left| \frac{2 \exp (0.5)}{|d_{ij}|} \cdot \frac{1}{2} \right| \right) \]
Tuse: \( \| c^3 \| < \sqrt{\lambda_{\text{max}}} |w_j| \left( \frac{2 \exp (0.5)}{|d_{ij}|_{\text{min}}} \right) \)
Then, we have:
\[ \eta d = \eta w \left( \frac{|d_{ij}|_{\text{min}}}{2 |w_j| \max \left| \frac{2 \exp (0.5)}{|d_{ij}|_{\text{min}}} \right|} \right)^2 \]

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